WADC TECHNICAL REPORT 52-56

A0-40% OF OR

AN APPROXIMATE METHOD FOR THE CALCULATION OF NONSTATIONARY AIR FORCES AT SUBSONIC SPEEDS



HENRY E. FETTIS
FLIGHT RESEARCH LABORATORY

MARCH 1952

Reproduced From Best Available Copy

WRIGHT AIR DEVELOPMENT CENTER

20020104145

NOTICES

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government procurement operation, the United States Government thereby incurs no responsibility nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

The information furnished herewith is made available for study upon the understanding that the Government's proprietary interests in and relating thereto shall not be impaired. It is desired that the Judge Advocate (WCJ), Wright Air Development Center, Wright-Patterson Air Force Base, Ohio, be promptly notified of any apparent conflict between the Government's proprietary interests and those of others.

AN APPROXIMATE METHOD FOR THE CALCULATION OF NONSTATIONARY AIR FORCES AT SUBSONIC SPEEDS

Henry B. Fettis
Flight Research Laboratory

March 1952

E. O. No. 459-41

Wright Air Development Center Air Research Development Command United States Air Force Wright-Patterson Air Force Base, Ohio

FOREWORD

This report was originally issued under the designation of OAR Technical Report #5, and contains the results of research on the problem of the calculation of oscillatory lift and moment coefficients which act on a two-dimensional airfoil moving at subsonic speeds. The work was begun and partly completed while the author was associated with the Dynamics Branch of the Air-craft Laboratory, Wright Air Development Center, under E. 0. 459-41. The author, who was also the project engineer, completed the research while a member of the Applied Mathematics Research Section of the Flight Research Laboratory, Wright Air Development Center. The new edition is being issued for the purpose of correcting numerous errors in the original, as well as meeting the demand for additional copies.

The author wishes to acknowledge the assistance of Mr. Hewitt S. Toney, then of the Dynamics Branch, Aircraft Laboratory, and presently of the Computation Research Section, of the Flight Research Laboratory, in developing many of the formulae and in carrying out the numerical calculations.

ABSTRACT

The present report explains and illustrates a method of computing the non-stationary forces and moments on an oscillating airfoil at subsonic speeds. The process is based on the well known Possio integral equation relating the pressure on the airfoil to the normal velocity.

Part I of the report contains the theoretical development which leads to the required equations for determining the lift and moment.

In Part II the method of Part I is applied to the computation of the aerodynamic lift and moment coefficients for four principal degrees of freedom of the airfoil, these being:

- a. Translation of the complete chord of the airfoil in a direction normal to the forward velocity (positive down).
- b. Rotation of the entire chord about the forward quarter-chord point (positive for increasing angle of attack).
- c. Translation of the portion of the airfoil extending from an arbitrary point to the trailing edge, in a direction normal to the forward velocity.
- d. Rotation about an arbitrary point of that portion of the airfoil extending from that point to the trailing edge.

The appendices contain the detailed mathematical derivation of the various formulae involved in the problem.

PUBLICATION REVIEW

Manuscript Copy of this report has been reviewed and found satisfactory for publication.

FOR THE COMMANDING GENERAL:

LESLIE B. WILLIAMS

Colonel, USAF

Chief, Flight Research Laboratory

Research Division

TABLE OF CONTENTS

I Sta	tement of the Problem and Method of Solution	1
II Res	ults of Numerical Calculations	11
Conclusion	ons - Recommendations	25
Bibliogra	aphy	26
APPENDIX		
I	Evaluation of Certain Integrals	28
II	Evaluation of $\int_{\mathcal{R}}^{c',u_{\mathcal{R}}} \varphi_{n}(z)dz$, $\int_{\mathcal{R}}^{c'} \varphi_{m}(z)dz$	34
III	Evaluation of $\mathcal{B}_{g}(x)$, $\mathcal{B}_{g}(x)$	37
IV	The Function $\int_{\mathcal{A}} (\mathcal{U}, b)$	42
V	The Function $\mathcal{I}_{n}(\mathcal{A}, \mathcal{V}, e)$	49
VI	A Derivation of the Inversion Formula for the Equation: $f(z) = \frac{1}{\pi} / \frac{I(z) dz}{x - z}.$	59
VII	The Possio Kernel and its Approximate Representation as a Polynomial.	62
VIII	Auxiliary Tables	72
Distribut	tion List	74

LIST OF TABLES AND FIGURES

Table	
(1.01)	Summary of the coefficients A_{ij}
(2.01)	The approximating coefficients $\mathcal{A}_o, \mathcal{A}_i$
(2,02)	The coefficients A_{ij}
(2.03)	The coefficients \mathcal{B}_{i}
(2.04)	Coefficients of total lift and moment
(2.05)	The coefficients $A_{lj}(x)$
(2.06)	The coefficients $\mathcal{B}_{j'}(z)$
(2.07)	Control surface lift and moment coefficients 2
	Lift and moment coefficients computed from Dietze 3
	Values of $\sqrt{\frac{1+\xi}{1-\xi}} d\xi$
(Al _• 02)	Values of in e in cos z dz
	Values of $e^{-i\mu\xi}/-\xi^2 d\xi$
(Al.04)	Values of $\int_{\mathcal{Z}} e^{-i\mu \chi} \sqrt{1-\xi^2} \chi d\chi$
(A3.01)	The coefficients Q_i , R_i
(A4.01)	Values of $\int_{n} (-\mu, \cos^{2}x)$

Table (A5.01)	Values of $\mu F'(\mu, x, e) \cdots 58$
Table (A5.02)	Values of I ₀ (u, x, e) · · · · · · · · · 58
Table (A5.03)	Values of $\mathcal{I}_{,(u,z,e)}$
Table (A5.04)	Values of $\mathbb{Z}_2(u,x,e)$
Table (A7.01)	(Reproduced from Reference 3) 68
Table (A8.01)	The function $\mathcal{T}(\boldsymbol{\omega})$
Table (A8.02)	eine
Table (48.03)	$\mathcal{J}_{p}(u)$ 73
Fig. (A7.01)	The non-singular kernel difference $\vec{K}(\lambda,z)$ 69
Fig. (A7.02)	Real part of α , and α , vs. ω 70
Fig. (A7.03)	Imaginary part of & and & vs & 71

TABLE OF SYMBOLS

Constants

ω	- "Reduced frequency", \(\operatorname{\operatorname{N}} \) where \(\operatorname{V} \) is the frequency of oscillation, \(\operatorname{D} \) the semichord, and \(V \) the forward velocity.
λ	- Mach number; $\lambda = V_{\sqrt{5}}$ where V_{5} is velocity of sound.
p	- Air density.
M	- Parameter defined by $\mu = \frac{\lambda^2 \omega}{\lambda - \lambda^2}$
×	- Chordwise coordinate, referred to semichord as unity.
8	- Chordwise variable of integration.
e	- Coordinate of control surface leading edge.
W	- Farameter defined by $W = \frac{\lambda \omega(x-Y)}{1-\lambda^2}$.
2	- Variable of integration. Also used in Appendix VII to designate ω (2-1)
ø	- Variable defined by $E = cos \phi$.
Ø	- Variable defined by $x = \cos \theta$.
E	- Variable defined by €=cos€.
or _e	- Coefficient of $\omega(x-\xi)^{\Re}$ in polynomial approximation of \mathcal{R} (cf. equation 1.16).
a _R	- Constants defined by equation (A2.03).
\mathcal{P}_{n}^{m}	- Constants defined by equation (A2.04) .

Functions

$$T(\omega) - \text{Function defined by Kussner; } T(\omega) = \frac{H_i^{(2)}(\omega) + iH_o^{(2)}(\omega)}{H_i^{(2)}(\omega) - iH_o^{(2)}(\omega)}$$

$$\Lambda(\theta, \varphi)$$
 - Function defined by Schwartz: $\Lambda(\theta, \varphi) = \frac{1}{2} \ln \frac{1 - \cos(\theta + \varphi)}{1 - \cos(\theta - \varphi)}$

$$W(x)$$
 - Downwash distribution across chord.

$$K(o, Z)$$
 - Kernel of the Possio integral equation when $\lambda = 0$.

$$\vec{K}(\lambda,z)$$
 - Non-singular kernel as defined by equation (1.04).

$$J_{\beta}(u,\theta)$$
 - Function defined by: $J_{\beta}(u,\theta) = \int_{0}^{\infty} e^{i\mu \cos \theta} \cos \theta d\theta$

$$I_p(M,z,e)$$
 - Function defined by $I_p(M,z,e) = \frac{e^{-iMz}(e-e)\Lambda(\cos z,\cos z)dz}{x}$

$$F(u, o, c)$$
 - Function defined by $F(u, o, c) = \int_{0}^{b} \frac{1 - e^{-ix(c \cdot s \cdot q - c \cdot s \cdot c)}}{c \cdot s \cdot q - c \cdot s \cdot c} dq$

Functions (continued)

Qx(w,e)	-	Coefficients defined by equation (A3.01)
Rx(w.e)	-	Coefficients defined by equation (A3.04)
$U_{\Lambda}(\theta, \epsilon)$	-	Function defined by equation (45.32)
Aij(x)	-	Function defined by equation (1.22)
Aii	-	$A_{ij} = A_{ij}(-1)$
B; (x)	-	Function defined by equation (1.22)
\mathcal{B}_{i}	•	$\mathcal{B}_{f} = \mathcal{B}_{f}(-1)$
An(M)	-)	
Bh (M)	- (Coefficients in series expansion of $J_p(\mu,\theta)$
Ch(M)	- ((See equations A4.17, 21, 24, 26)
Dr(N)	- <i>J</i>	
Un(2)	•	Polynomial defined by equation (1.17)
$\Phi_n(x)$	•	Function defined by equation (1.18)

INTRODUCTION

The question of the effect of compressibility on flutter calculations has been the subject of numerous investigations. The first approach to the problem was the use of the well known Prandtl-Glauert correction factor by which the aerodynamic force is increased in the ratio $1:\sqrt{-\lambda^2}$ where λ is the Mach number. Since this correction changes the magnitude of the aerodynamic force but not the phase, it is evident that such a correction, while satisfactory for the stationary case, cannot be relied upon in the non-stationary case where the phase change is one of the most important factors.

In 1938 Possio (Ref. 11) wrote down the relation between the pressure distribution over a chordwise element of the airfoil and the total normal velocity at any point (downwash), taking into account the compressibility of the medium, in the form of an integral equation of the first kind which now bears his name. The same equation was derived independently by Kussner in 1940 (Ref. 4). Since no explicit solution of the equation was evident (nor has since been found) recourse to an approximate solution was made. Possio obtained a solution by assuming that if the equation were satisfied at a finite number of points on the chord, the results should approximate the exact values. Using this method, Possio was able to calculate total lift and moment coefficients for values of the reduced frequency less than .6, and for motions of the airfoil corresponding to rigid translation and rotation of the complete chord. Possio's results were later checked and extended by Frazer and Skan (Ref. 5). This method, now known as the collocation method, results in a system of linear equations with as many unknowns as points for which the equation is satisfied. Since the coefficients in these equations are complex numbers, it is evident that such a solution is long and tedious if a large range of parameters is to be considered. Further, it is not possible to duplicate accurately by this method the conditions of a discontinuous downwash which occurs when a control surface is added to the airfoil.

A different approach to the problem was made by Schade (Ref. 12) and Eichler (Ref. 13), in which expansions of both sides of the equations were made in terms of known functions. Schade employed Legendre functions while Eichler used a trigonometric series. By limiting the expansions to a finite number of terms and equating like coefficients, the problem

was again reduced to the solution of a system of linear equations. Thus this method, while perhaps more accurate than the collocation method, was still too laborious to be practical. (Schade indicated that the case of a discontinuous downwash could be handled by the introduction of the proper singularity in the pressure distribution. He did not, however, present any numerical results for the non-stationary case).

In 1943 a new departure was made by Dietze (Ref. 3) who noted that the difference between the kernel of the integral equation in the compressible case and that of the incompressible case was small compared to the actual value of the kernel. Thus, using the known incompressible solution as a starting point, Dietze was able to compute by an iterative process the solution to the compressible problem. By this method Dietze obtained a number of results for the case of control surface rotation. While the details of Dietze's calculations were not available to the author, it appears that a large amount of labor would be required to obtain a complete set of aerodynamic coefficients covering the range of parameters required for conventional aircraft.

The present method resembles Dietze's in that the incompressible solution is used as a starting point. It is, however, not an iterative process but results in a closed solution based on replacing the non-singular portion of the kernel by a polynomial. The question of the rapidity of the convergence of the pressure distribution series is no longer of any concern, and the only discrepancy between the solution obtained and the exact solution lies in the difference existing between the actual kernel remainder and the approximation. The remainder is approximated over the required interval by minimizing the total "mean square" error over the interval. The numerical results indicate that this approximation is satisfactory even when an apparently large discrepancy exists between the kernel difference and the polynomial approximation.

PART I

STATEMENT OF THE PROBLEM AND METHOD OF SOLUTION

The problem of determining the lift and moment on an oscillating airfoil in compressible subsonic flow was reduced by Possio to the solution of an integral equation of the first kind, which relates the pressure differential over the airfoil chord to the downwash at any point on the chord. The equation may be written in the form

(1.01)
$$W(x) = \omega / K[\lambda, \omega(x-z)] Z I(z) dz$$

where λ is the Mach number, $k(\lambda)$ is the downwash at any point, expressed as a function of the distance x (positive aft) of the point from the mid-chord, ω is the "reduced frequency" and x(t) is equal to p times the pressure distribution across the chord.

The distances χ and ξ are non-dimensional with the semi-chord taken as unity. The explicit form of the nucleus κ is given elsewhere (see for example, App. 7). In the present treatment only the singularities and the numerical values of κ are required. As shown in other investigations of the subject, $\kappa(\chi, \xi)$ has the following form near $\kappa \in \Sigma$:

(1.02)
$$K[\lambda,\omega(x-z)] = \frac{\sqrt{1-\lambda^2}}{2\pi} \frac{1}{\omega(x-z)} + \frac{i}{2\pi\sqrt{1-\lambda^2}} L_{op}[\omega(x-v)] + K_i[\lambda,\omega(x-z)].$$

where K_{ℓ} has no singularities. For $\lambda = 0$,

(1.03)
$$K[Q\omega(x-z)] = \frac{1}{2\pi} \frac{1}{\omega(x-z)} + \frac{L}{2\pi} \frac{\log|\omega(x-z)|}{\log|\omega(x-z)|}.$$

Since the solution of equation (1.01) is known for the incompressible case where $\lambda = 0$, it is logical to attempt a solution for $\lambda \neq 0$ by making use of the results already obtained for the incompressible case.

To this end, the nucleus is written in the form

(1.04)
$$K[\lambda, \omega(x-\xi)] = \frac{1}{\sqrt{1-\lambda^2}} K[o, \omega(x-\xi)] + \frac{\lambda^2}{2\pi\sqrt{1-\lambda^2}} \left[\frac{1}{\omega(x-\xi)} \right] + \widehat{K}[\lambda, \omega(x-\xi)]$$

Clearly, \widehat{K} is non-singular and may be approximated to a good degree of accuracy by a polynomial. The advantage obtained by the present treatment lies in the fact that all singularities in the pressure distribution are taken care of by means of the incompressible solution, and that the resulting solution is obtained without the use of the usual series representation for $\mathbb{Z}(\mathcal{E})$. Thus the question of the rapidity of convergence of such a series does not enter. Further, for low values of ω , a satisfactory approximation to \widehat{K} is obtained by retaining only the constant and linear terms of the polynomial.

Placing for K the alternative expression as given by (1.04)

$$(1.05) W(x) = \frac{\omega}{\sqrt{1-\lambda^2}} \int_{-\lambda}^{\lambda} K[o,\omega(x-E)] II(E) dE + \frac{\lambda^2}{2\pi\sqrt{1-\lambda^2}} \int_{-\lambda}^{\lambda} \frac{II(E)dE}{x-E} + \omega \int_{-\lambda}^{\lambda} [\lambda,\omega(x-E)] II(E) dE$$

According to the work of Kussner (Ref. 1), the solution to the equation

(1.06)
$$\omega \int_{\mathbb{R}} K[o, \omega(x-E)] \mathbb{I}(E) dE = f(x)$$

subject to the Kutta condition that $\mathbb{Z}(\xi)$ remain finite at $\xi = /$ is given by

$$(1.07) II(x) = \int_{\gamma}^{\gamma} G(x, z) f(z) dz$$

where
$$G(x,z) = -\frac{2}{\pi} \left[i\omega \Lambda(x,z) + \sqrt{\frac{1-x}{1+x}} \sqrt{\frac{1+z}{1-z}} \left\{ C(\omega) + \frac{1}{z-x} \right\} \right]$$

(1.08)
$$\Lambda(x,z) = \frac{1}{2} \log \frac{1 - \chi z + \sqrt{1 - \chi^2} \sqrt{1 - z^2}}{1 - \chi z - \sqrt{1 - \chi^2} \sqrt{1 - z^2}}; C(\omega) = \frac{T(\omega) - 1}{z} = \frac{-\frac{1}{2} (2)}{\frac{1}{2} (2)(\omega) - i H_0^{(2)}(\omega)}$$

Since T(w) = 1 for w = 0, this gives the additional result that if

(1.09)
$$\frac{1}{\pi} \int \frac{\underline{\pi}(\xi) d\xi}{x - \xi} = f(x)$$

and II(1) is finite, then

(1.10)
$$\sqrt{\frac{1+x}{1-x}} \, \mathbb{Z}(x) = \frac{2}{\pi} \int_{x-z}^{1} \sqrt{\frac{f(z)}{x-z}} \, dz$$

or, what is equivalent

(1.11)
$$\int \sqrt{\frac{1+z}{1-z}} \frac{dz}{z-x} \int \frac{II(z)}{z-z} dz = \pi^2 \sqrt{\frac{1+x}{1-x}} II(x)$$

It can be seen that if equation (1.05) is rewritten in the form

$$(1.12) \frac{\omega}{\sqrt{-\lambda^2}} \int_{\zeta} K[o,\omega(x-t)] II(t) dt = W(x) - \frac{\lambda^2}{2\pi\sqrt{1-\lambda^2}} \int_{\zeta} \frac{II(t) dt}{x-t} \omega \int_{\zeta} K[\lambda,\omega(x-t)] II(t) dt$$

it can be formally regarded as a special case of equation (1.06) with f(x) replaced by the entire right side of (1.12). Thus application of equation (1.07) gives the result

$$\frac{II(x)}{\sqrt{1-\lambda^2}} = II_o(x) + \frac{\lambda^2}{II_o(x)} \int_{-1}^{1} \left[i\omega \Lambda(x,z) + \frac{1-x}{1-x} \int_{1-x}^{1+x} \frac{1}{1-x} \left\{ \frac{1}{z-x} + C(\omega) \right\} \right] \frac{II(z)dz}{x-z}$$

$$(1.13)$$

$$-\omega \int_{-1}^{1} G(x,z)dz \int_{-1}^{1} \left[\lambda_1 \omega(z-z) \right] II(z)dz$$

where $\Pi_0(x) = \int_{-\infty}^{\infty} G(x,z) W(z) dz$ is the incompressible pressure distribution corresponding to the given downwash W(z). Making use of equation (1.11) and the following results established in Appendix I.

$$(1.144) \quad \frac{1}{\pi} \int \sqrt{\frac{1+z}{1-z}} \, dz \int \frac{II(z)dz}{z-z} = \int_{-1}^{1} II(z)dz$$

$$(1.14B) = \int_{-1}^{1} \Lambda(x,z) dz \int_{-1}^{1} \frac{II(t)dt}{z-t} = \cos^{2}x \int_{-1}^{1} I(t)dt - II \int_{2}^{1} I(t)dt$$

gives

$$II(x) + ca II(t) dt = \frac{II_0(x)}{\sqrt{1-\lambda^2}} + \left\{ \frac{\lambda^2 C(\omega)}{\pi (1-\lambda^2)} \sqrt{\frac{1-\kappa}{1+\kappa}} + \frac{i\kappa}{\pi} \cos^2 \kappa \right\} / II(t) dt$$

(1.15)

$$-\frac{\omega}{\sqrt{1-\lambda^2}}\int_{-1}^{1}G(x,z)dz\int_{-1}^{1}K[\lambda,\omega(z-z)]II(E)dE,$$

with $M = \frac{\lambda^2 \omega}{1 - \lambda^2}$.

The non-singular nucleus may evidently be approximated to the desired degree of accuracy by a polynomial of degree n:

$$||\tilde{R}[\lambda, \omega(z-z)| = \alpha_0 + \alpha_1 \omega(z+z) + \alpha_2 \omega^2(z-z)^2 + \dots + \alpha_n \omega^n(z-z)^n$$

$$= u_0(z) + u_1(z)\xi + u_2(z)\xi^2 + \dots + u_n(z)\xi^n$$

where

$$46(2) = 90 + 9162 + 91624 + --- + 91627$$

$$(1.17) \quad \mathcal{U}_{1}(z) = -\alpha_{1}\omega - 2\alpha_{2}\omega^{2}z - 3\alpha_{3}\omega^{2}z^{2} + \dots - n\alpha_{n}\omega^{n}z^{n-1}$$

$$\mathcal{U}_{2}(z) = \alpha_{2}\omega^{2} + 3\alpha_{3}\omega^{3}z + \dots + \frac{n(n-1)}{2!}\alpha_{n}\omega^{n}z^{n-2}$$

$$\mathcal{U}_{3}(z) = -\alpha_{3}\omega^{3} - 4\alpha_{1}\omega^{4}z + \dots - \frac{n(n-1)(n-2)}{3!}\alpha_{n}\omega^{n}z^{n-3}$$

WADC TR 52-56

The last term in equation (1.15) then becomes

(1.18)
$$\phi_0(x) \int_{\mathcal{I}} I(\xi) d\xi + \phi_1(x) \int_{\mathcal{I}} I(\xi) \xi d\xi + --- + \phi_n(x) \int_{\mathcal{I}} I(\xi) \xi^n d\xi$$

with $\phi_m(x) = \int_{\mathcal{I}} G(x, z) \ell_m(z) dz$, $m = 0, 1, 2 --- \pi$.

Equation (1.15) may now be written

$$\underline{\underline{\underline{T}}}(x) + i\mu \int_{\mathcal{A}} \underline{\underline{T}}(\xi) d\xi = \underline{\underline{T}}(N) + \underbrace{\lambda^2 c(\omega)}_{\overline{T}(1-\lambda^2)} \underbrace{I-x}_{\overline{T}} + \underbrace{i\pi}_{Cos} \underbrace{\pi}_{Cos} - \omega \underbrace{\overline{D}_o(z)}_{\overline{I-\lambda^2}} \underbrace{\underline{T}(e) d\xi}_{\overline{I}}$$

(1.19)
$$-\omega \frac{\Phi_{\ell}(x)}{\sqrt{\ell-\lambda^2}} \int \underline{\pi}(t) t \, dt + \cdots - \omega \frac{\Phi_{n}(n)}{\sqrt{\ell-\lambda^2}} \int \underline{\pi}(t) t \, dt$$

This equation may be solved as a differential equation in $y = \int_{x}^{x} Z(t) dt$ by introducing the integrating factor e^{-ixx} , viz.

$$e^{i\mu \chi} I (t) dt = \sqrt{I - \lambda^2} \int_{X} I (t) e^{-i\mu \xi} dt$$

$$+ \left\{ \frac{\lambda^2 C(\omega)}{\pi (I - \lambda^2)} \int_{I + \Sigma} e^{i\mu \xi} dt + \frac{i\mu}{\pi} \int_{Cos} e^{-i\mu \xi} dt - \frac{\omega}{\sqrt{I - \lambda^2}} \int_{X} e^{-i\mu \xi} dt \right\} \int_{I + \Sigma} I (t) dt$$

$$- \frac{\omega}{\sqrt{I - \lambda^2}} \int_{X} e^{-i\mu \xi} I (t) d\xi \int_{I + \Sigma} I (t) dt + \cdots - \frac{\omega}{\sqrt{I - \lambda^2}} \int_{X} e^{-i\mu \xi} I (t) dt \int_{I + \lambda^2} I (t) dt$$

Setting Z = -1 in the above expression, we obtain a linear equation relating the $(\pi + \ell)$ unknowns $\int II(\ell) \delta \ell$, $\int II(\ell) \ell \delta \ell$.

where

$$A_{00} = e^{iA} - \frac{\lambda^{2}C(\omega)}{\pi(I-\lambda^{2})} \left[e^{-iA\xi} \frac{1-\xi}{I-\xi} d\xi - \frac{iA}{\pi} \right] e^{-iA\xi} \cos \xi d\xi + \frac{\omega}{I-\lambda^{2}} \left[e^{-iA\xi} \frac{\partial}{\partial \xi} (\xi) d\xi \right].$$

$$A_{0n} = \frac{\omega}{\sqrt{I-\lambda^{2}}} \left[e^{-iA\xi} \frac{\partial}{\partial \eta} (\xi) d\xi \right], \quad n > 0$$

$$B_{0} = \int e^{-iA\xi} \frac{\partial}{\partial \eta} (\xi) d\xi$$

Expressions for these coefficients are obtainable in terms of Bessel and other known functions (See Appendix I, II, III).

The n additional equations required for the complete determination of the unknowns are obtained by multiplying equation (1.19) by x^{n} n = 0, 1, 2 - -(n-1) and integrating between the limits -1 and 1. Then since

(1.23)
$$\int_{-\pi}^{\pi} dx \int_{\pi}^{\pi} I(z) dz = \frac{(-)^{\frac{1}{2}}}{\pi^{\frac{1}{2}}} \int_{\pi}^{\pi} I(z) dz + \int_{\pi}^{\pi} \frac{E^{\frac{1}{2}\pi} II(z)}{\pi^{\frac{1}{2}}} dz$$

the following equations result

$$\begin{cases}
A_{oo}X_{o} + A_{oi}X_{i} + \cdots + A_{on}X_{n} = B_{o}/\sqrt{1-\lambda^{2}} \\
A_{io}X_{o} + A_{ii}X_{i} + \cdots + A_{in}X_{n} = B_{i}/\sqrt{1-\lambda^{2}} \\
A_{no}X_{o} + A_{ni}X_{i} + \cdots + A_{nn}X_{n} = B_{n}/\sqrt{1-\lambda^{2}}
\end{cases}$$

WADO TR 52-56

The (new) equations may be solved simultaneously to determine the quantities

The first two of these give directly the lift and mid-chord moment over the entire chord. In the case of a wing-aileron combination, the lift on the control surface extending from $\xi = \kappa$ fo $\xi = 1$ is also required, which is found from equation (1.20) after substitution of the known values for X_0, X_1, \dots, X_n

The partial mid-chord moment is found in a similar manner by integrating equation (1.19) from x to 1, with the aid of the relation

(1.25)
$$\int_{\pi}^{t} dx \int_{\pi}^{t} I(\xi) d\xi = \int_{\pi}^{t} (\xi - x) II(\xi) d\xi$$

Equation (1.25) may be applied to a wing-control surface combination by regarding x as the coordinate of the control surface leading edge, since the right side is precisely the moment about the leading edge.

The required relations are summarized by the following equations:

Total lift on control surface -

(1.26)
$$e^{-i\mu x} II(E) dE = \frac{1}{\sqrt{1-\lambda^2}} B_o(x) - A_o(x) X_o - A_o(x) X_t - \dots - A_o(x) X_n$$
.

Total moment about the control surface leading edge -

$$i\mu \int_{\chi}^{1} (Z-\chi) II(E) dE = \frac{1}{\sqrt{1-\lambda^{2}}} B_{i}(x) - \int_{Z}^{1} I(E) dE$$

$$-A_{i,0}(x) X_{0} - A_{i,1}(x) X_{i} + \cdots - A_{i,n}(x) X_{n}.$$

Where A_{0j} (x) and B_{0} (x) designate the respective quantities appearing in equation (1.20); A_{ij} (x) and B_{1} (x) denote the corresponding quantities obtained from equation (1.19) by integration from x to 1.

The expressions for the A_{ij} [i,j=0,1,2,3] and $A_{ij}(x)$ [i=0,1,j=0,1,2,3] are listed in Table (1.01). The various integrals involved are evalued in Appendix I, II, while the evaluation of the B_j is carried out in Appendix III for the following four types of motion:

- a. Translation of the entire chord.
- b. Rotation of the entire chord about the forward quarter chord point.
- c. Translation of the control surface.
- d. Rotation of the control surface about its leading edge.

For routine calculations the following procedure is suggested:

a. Calculation of all quantities which do not depend on the polynomial approximation. These include the following:

Aoo	Aoo(x)	\mathcal{B}_o	$\mathcal{B}_o(x)$
Ã,o	Aio(x)	\mathcal{B}_{ℓ}	$\mathcal{B}_{a}(\mathbf{z})$

and the coefficients of a_A^{77} in equation (A2.08).

- b. Determination of the approximating coefficients $\alpha_0, \alpha_1, \dots, \alpha_n$ as defined by equation (2.03).
- c. Calculation of $\mathbb{R}^m [m=0,1,\dots,n-1,n=0,1,\dots]$ as defined by (A2.05).
 - d. Calculation of and from equation (A2.03).
- e. Calculation of the integrals involving from equations (A2.08) (A2.12).
 - f. Calculation of A_{ij} , $A_{ij}(x)$ as given in Table (A1.01).
- g. Solution of the basic equations (Al.24) to determine the unknown quantities $X_0, X_1, ---, X_n$. The first two of these are preportional respectively to the total lift and total moment about the mid-chord.
- h. Resubstitution of the above quantities into equations (1.25) and (1.27) to determine the lift and moment over any portion of the chord.

TABLE (1.01)

SUMMARY OF THE COEFFICIENTS Ai; (*)

$$\begin{split} \hat{A}_{ij} &= \bar{A}_{ij} + \bar{A}_{ij}, \text{ where} \\ \bar{A}_{oo} &= \bar{J}_{o}(\underline{\mu}) - \frac{\lambda^{2}c(\omega)}{1-\lambda^{2}} \left[\bar{J}_{o}(\underline{\mu}) + i \, \bar{J}_{i}(\underline{\mu}) \right]^{2}, \, \bar{A}_{oj} &= 0 \quad , j > 0 \\ \bar{A}_{10} &= 1 - \frac{\lambda^{2}c(\omega)}{1-\lambda^{2}} \; ; \quad \bar{A}_{11} &= i \underline{\mu} \quad \bar{A}_{1j} &= 0 \quad , j > 1 \\ \bar{A}_{20} &= -\frac{i \underline{\mu}}{2} \quad ; \quad \bar{A}_{21} &= 1 \quad ; \quad \bar{A}_{22} &= \frac{i \underline{\mu}}{2} \quad ; \quad \bar{A}_{2j} &= 0, j > 2 \\ \bar{A}_{30} &= -\frac{\lambda^{2}c(\omega)}{2(1-\lambda^{2})} \; ; \quad \bar{A}_{3i} &= 0 \quad ; \quad \bar{A}_{32} &= 1 \quad ; \quad \bar{A}_{33} &= \frac{i \underline{\mu}}{3} \; ; \quad \bar{A}_{3n} &= 0 \quad , j > 3 \\ \bar{A}_{0j} &= \frac{\omega}{\sqrt{1-\lambda^{2}}} \int_{C_{i}}^{1} e^{-\frac{i \underline{\mu}}{2}} \underbrace{\int_{i}^{1} e^$$

For the integrals involving see Appendix II.

WADC TR .52-56

PART II

RESULTS OF NUMERICAL CALCULATIONS

In the present calculations, the lift and moment coefficients have been calculated for the case where $\lambda = .7$ and $\omega \le .5$. Only the constant and linear terms have been retained in the kernel difference K as defined by equation (1.04). The difference is plotted in figure (A7.01) as a function of $Z = \omega(x - K)$, from which it can be seen that for the imaginary part, a straight line approximation is adequate over the interval $\left[-/ \le Z \le /\right]$ corresponding to the range $\left[-0 \le \omega \le .5\right]$ for the reduced frequency. For the real part, this approximation is also considered satisfactory since the magnitude of this portion over the interval is small compared to the magnitude of the actual kernel. The line used is that one which gives for K the best approximation in the "least squares" sense, i.e., for each ω the coefficients α_s and α_s are so determined that

(2.01)
$$E(\omega) = \int_{-\alpha}^{\alpha} \left[\vec{K} - (\alpha_o + \alpha_i, z) \right]^{\alpha} dz$$

is a minimum, where $a = 2\omega$. This condition is satisfied provided

$$\frac{\partial E}{\partial \alpha_0} = 0 , \frac{\partial E}{\partial \alpha_i} = 0 ,$$

which leads for the determination of d, and d, to the relations

(2.03)
$$\alpha_{i} = \frac{1}{2a} \int_{-a}^{a} \vec{R}(z) dz$$

$$\alpha_{i} = \frac{3}{2a^{3}} \int_{-a}^{a} \vec{R}(z) z dz$$

These equations define α , and α , as continuous functions of ω . The integrations are carried by the procedure described in Appendix VII and the results are listed in Table (2.01). α , and α , are plotted in figures (A7.02) and (A7.03) as functions of ω .

TABLE 2:01 VALUES OF α , and α ,

ပ		v d,		wax,
	REAL	IMAGINARY	HBAL	INAGINARY
•05	0	0025331	•000795	0004201
.10	000005	005079i	.002425	0016711
•20	000041	0102771	•006601	0065781
•30	000161	0157031	•010565	0143771
. 40	000453	-•05171651	•013190	0245231
. 50	001053	0276411	.013779	0363091

The next step is the evaluation of the coefficients A_{ov} , A_{ov} , A_{ov} , and A_{ov} . These are tabulated in Table (2.02) for $a_{ov} = a_{ov} = a_{ov}$.

In the evaluation of the \mathcal{J}_i , the factor \mathcal{H}_{ρ}_{b} times the non-dimensional amplitude is removed in order to obtain lift and moment coefficients comparable to those tabulated in reference 6. Values of these quantities are listed in Table (2.03).

TABLE (2.02)

THE COEFFICIENTS λ_i ; FOR VARIOUS VALUES OF ω - $\lambda = .7$

w	Aoo	Aoi	Aco	A.,
.05	1.08269+.15000i	.0060780039301	1.086884+.14789i	.005980+.0439661
.10	1.14694+.218511	.0166590140811	1.159400+.210711	.015933+.0812341
.20	1.21915+.299211	.0417360437991	1.25440 0 +.27350i	+03 7007 + .144 9 371
.30	1.24357+.36271i	-070906 0794841	1.307580+.314461	.057738+.2014261
.40	1.23995+.426641	.1061301192251	1,337930+,353741	.079972+.2533581
.50	1.21895+.494211	.1493891631191	1.355730+.396131	.104048+ .3006271

TABLE (2.03)

VALUES OF D. FOR VARIOUS &; \(\lambda = .7\)

MODE OF MOTION	h Translation (A TRANSLATION OF ENTIRE CHORD		M ABOUT QUARTER CHORD FOIRT
ω	Box / 4/6 +2 10	Br / 805 8/6.	Butaphy .	Bin/11/063 42 do
.05	-3.3500-36.46491	-4.2256-36.3604	-733.628+30.522901	-731.933+48.15521
.10	-1.6408-16.76551	-2.4460-16.63841	-170.274380251	-169.339+7.82161
.20	1762-7.38921	8862-7.27581	-38.0994-6.547901	-37.765-2.84481
.30	.45113-4.1710i	1955-4.43311	-15.5592-6.086061	-15.4726+3.781581
.40	.77636-3.16621	.1751-3.12491	-8.10142-5.200121	-8,13715-3,562651
.50	.96094-2.39641	.3972-2.391#1	-4.98424-4.433751	-4.88636-3.18608 <u>f</u>

CONTROL SURFACE TRANSLATION		Control Surface	ROTATION
Box for 62 yes.	B12/11/88220	304/11pb3v2po	Bir/ripb3v2A.
-2.85070-22.21350	- 2.98 699- 22 .14336	-445.2 89 40+49.47210	-443.90690+52.22120
-1.80925-10.22309	-1.90310-10.13279	-102.89650+ 1 4.62350	-101.99990+15.59110
915826-4.525884	95319-4.43095	-22.99155+3.04556	+22.50450+3.26170
529040-2.786501	53255-2.69978	-9.51866+.8 216 5	-9.20616+.85853
325568-1.979462	30687-1.90305	-5.10957+.14755	-4.88799+.12105
206246-1.523000	17162-1.45655	-3.16595 09 751	-2.97768+,15123
	-2.85070-22.21350 -1.80925-10.22309 915826-4.525884 529040-2.786501 325568-1.979462	-2.85070-22.21350 -2.98699-22.14336 -1.80925-10.22309 -1.90310-10.13279 915826-4.52588495319-4.43095 529040-2.78650153255-2.69978 325568-1.97946230687-1.90305	-2.85070-22.21350 -2.98699-22.14336 -445.28940+49.47210 -1.80925-10.22309 -1.90310-10.13279 -102.89650+14.62350 915826-4.52588495319-4.43095 -22.99155+3.04556 529040-2.78650153255-2.69978 -9.51866+.82165 325568-1.97946230687-1.90305 -5.10957+.14755

The equations for the total lift and moment are

(2.04)
$$\begin{cases} A_{\bullet o} / \Pi(z) dz + A_{oi} / \Pi(z) z dz = B_{o} / \sqrt{1-\lambda^{2}} \\ A_{io} / \Pi(z) dz + A_{ii} / \Pi(z) z dz = B_{i} / \sqrt{1-\lambda^{2}} \end{cases}$$

In order to obtain directly the moment about the quarter chord, these equations may be re-written in the form

$$(2.05) \left\{ \begin{bmatrix} A_{00} - \frac{1}{2} A_{01} \end{bmatrix} \int_{L_{1}}^{L_{1}} (\xi) d\xi + A_{01} \int_{L_{1}}^{L_{2}} (\xi) [\frac{1}{2} + \xi] d\xi = B_{0} / \int_{1-\lambda^{2}} (\xi) [\frac{1}{2} + \xi] d$$

The solution of the above equations results in values for the total lift and moment coefficients as listed in Table (2.04).

TABLE (2.04)

CONFFICIENTS OF TOTAL LIFT AND MOMENT

A=.7

Mode CF> Motion	A TRANSLATION OF ENTIRE CHORD		ROTATION ABOUT QU	X ARTER CHORD FOINT
•	$L_{h} = \frac{\int_{-\infty}^{\infty} I_{h}(t) dt}{V \rho b^{2} V^{2} h_{0}}$	Ma Tros vo	Ly = \(\int_{\text{T}}(\epsilon) \delta \text{T}_{\text{T}}(\epsilon) \delta T	Ma = SEXULTIGE RPB VER.
.05	-10.793-45.7 69 1	1.1%2441	-927.4+170.321	-4.0361 -38.1681
.10	-5.880-19.4371	1.0572791	-201.3+39.641	-2.1010-17.86491
.20	-2.361-7.9581	.9182991	-43.07+4.1471	9635-8.40041
.30	-1.102-4.7891	.8423101	-17.918071	-5962-5.44711
.40	520-3.4141	.7883261	-9.847-1.7871	451-4.01281
.50	217-2.6721	.7453461	-6.306-1.8931	3783-3.16971

MOTION	e		2- TRANSLATION OF CONTROL SURFACE		
6	$L_{p} = \frac{\int_{-\pi}^{\pi} f(x) dx}{\pi p b^{2} r^{2} p_{0}}$	Mp = [25,(c) [2+ 2] dz	L3 = \(\int_{2} \langle \text{(6) d2} \)	M2 = \(\int_{0} = \frac{\pi_{0} = \frac{\pi_{0}}{\pi_{0}} = \pi	
.05	-556.226+141.6661	-234.688-11.62831	-7.55258-27.6801	.34425-11.73771	
.10	-117.566+40.6061	-59.689-4.90781	-4.4527-11.60001	.25098-5.97151	
.20	-23.733+9.42351	-15.4232-1.96161	-2.1923-4. 588 61	.14680-3.08281	
.30	-9.3262+3.6604 1	-7.0532-1.11201	-1.3613-2.64701	.08426-2.10671	
.40	-4.8473+1.81681	-4.0644728411	96113-1.79381	.04039-1.607481	
.50	-2.9295+1.04321	-2.6554513461	73411-1.323811	.00645-1.299471	

Equations (1.25) and (1.27) may now be employed to calculate the forces and moments on the control surface, after first evaluating the quantities $A_{\circ\circ}(x)$, $A_{\circ\circ}(x)$, $A_{\circ\circ}(x)$, $A_{\circ\circ}(x)$, $A_{\circ\circ}(x)$, $A_{\circ\circ}(x)$, and $\mathcal{F}_{\circ}(x)$. In the example, the value x = x = x was used. The basic quantities are listed in Tables (2.05) and (2.06) and the results in Table (2.07).

* Here & denotes the coordinate of the control surface leading edge in the notation of Ref. 7.

TABLE (2.05)

THE COLFFICIENTS A:(z) FOR VARIOUS VALUES OF ω $z=e-\varepsilon$, $\lambda=-7$

ω	A00 (x) x10°2	Ao, (2) 310 +2
.05	.45570+.33840i	.03502022261
.10	.75200+ .212501	.09707077581
.20	.8738 2752i	:2650-, 23001
.30	.5970 67601	.5211 42251
.40	.1105 85571	.903970201
.50	451879121	1.4050-1.15081

ω	A10(x) x 102	An(x) 410°2
.05	.44420+ .353301	.03575021101
.10	.73640+ .262001	.10200070901
.20	.903515801	.293219 251
.30	.720554891	.594430951
.40	.332080831	1.056743581
.50	171491791	1.705162061

TABLE (2.06)

VALUES OF $\frac{260}{\sqrt{1-\lambda^2}}$ FOR VARIOUS ω_i ; $\varkappa=e^{-\lambda x}$, $\lambda=-?$

MODE OF -	~		ROTATION ABOUT QUARTER CHORD POI	
&	Bown Ppb Tho VI-2"	3. (A) APOVAOTI-A	B. (W) (& of 1-22	B, (x)
.05	246179-2.929692 1	148238-2.9361891	-59.01179-1.8626651	-58.91258-3.8346381
.10	094170-1.3404631	004521-1.3435981	-13.670495-2.3215861	-13.48092-3.228431
.20	0420375988151	.1214365875391	-3.123135-1.759751£	-2.85663-2.157831
.3 U	.1022013865891	.1772193579861	-1.356 597- 1.3492931	-1.05645-1.592061
.40	.1327412987041	.2071422523421	782840-1.0847471	46409-1.252711
.50	.1486182569681	.2250751931391	5324289049721	20158-1.02931

MODE OF -	Z TRANSLATION OF CONTROL SURFACE		ROTATION OF CONIROL SURFACE	
&	760 7. 11-X=	B, (4) / 10 / 2 / 2. 1-75	Ap6 Pp. Sign	B, (x)
.05	317587-6,037301	12367-6.044471	-120.9059+3.397501	-120.9469484571
.10	224897-2.9380941	03614-2.946421	-29.5092+.801101	-29.4919-1091751
.20	141457-1.4159481	.040566-1.421901	-7.17947+,0050541	-7.11113911991
.30	-,104009-,9256521	.074534927401	-3.17216-,111181	-3.08145714261
.40	0842816884761	.092758685721	-1.80065126511	-1.69822577921
.50	073168550421	.10368543251	-1.17588118991	-1.06674482371

		.,,		فالمستوعية والتناف في عليه بين بالأناف عند بالأم ويونون بين بين بين بالأناف والأناف والمناف وا
MODE OF	A TRANSLATION OF ENTIRE CHORD		ROTATION ABOUT QUARTER CHORD POINT	
*	7 - TPB 2 y 2 ho	The Top be so he	$R = \frac{\int_{e}^{1} II_{N}(e) de}{R \rho b^{2} V^{2} d_{0}}$	$T_{a} = \frac{\int_{e} (t-e) II_{n}(e) dt}{II_{p} b^{2} v^{2} d_{o}}$
.05	29362-2.698891	0533950975i	-54.3428660451	-10.685269781
.10	04530-1.191421	00456232961	-12.02504-2.65942	-2.34416588851
.20	.12209531441	.02770104161	-2.59931-2.098481	496794429 01
.30	.1769934362i	.038 20+. 068421	-1.05165-1.571271	1992432819i
.40	.19888271531	.04238053331	55034-1.235241	1005825929i
.50	.20661232361	.043 87 04 5661	32912-1.007471	05793209 40 1

MOLE CF -	Z TRANSLATION OF CONTROL SURFACE		A ROTATION OF CONTROL SURFACE	
•	$\frac{1}{3} = \frac{\int_{c}^{1} \pi_{2}(z) dt}{\pi \rho b^{2} v^{2} Z_{o}}$	$T_{\lambda} = \frac{\int_{e}^{1} (t-e) \pi_{\lambda}(e) I_{t}}{\pi \rho \delta^{2} y^{2} 20}$	$ \frac{\int_{c}^{r} \pi_{\rho}(\epsilon) d\epsilon}{\pi \rho h^{3} r^{2} \beta o} $	To te (t-c) IIp (t) de
.05	23729-5.892821	03 9 4098793i	-117.967+1.8400i	-19.7773+.1/3751
.10	08174-2.346521	0091547459i	-28.522/60103i	-4.752922373i
.20	.021/.5-1.381251	.010 69- .22922i	-6.92832801441	-1.1472720818i
.30	.053103913591	.01667151551	-3.05662636431	50/12158141
.40	.064404684951	.0187211354.1	-1.71943504451	28241123561
.5 0	.0685 0 5548401	.01942090881	-1.10263/10721	1900/10071

For comparison, some values of the above coefficients as computed in Reference 17 from Dietse's original data of Reference 3 are shown in Table (2.08). The control surface coefficients are somewhat incomplete and also sorrespond to a value of C=.52 so that only a qualitative comparison can be made. However, it appears that reasonably good agreement exists even for the higher values of a where only a rough approximation to the actual kernel was used.

In a subsequent report, an extended range of control surface chords is to be considered. It is also planned to check the present results for the higher values of ω by employing a cubic approximation for K. This approximation should hold for values of ω as high as 1.

TABLE (2.08)

LIFT AND MOMENT CONFFICIENTS COMPUTED FROM DIETZE $\lambda = .7$

ω	Lh	Mh	L«	Ma
.2		+.8110435860j +.8408132444j +.8738929900j +0.93050 - 0.28700j +1.0560025200j	-18.0322284078j -43.15500 + 4.14500j	39900 - 3.407603 43375 - 4.222503 55589 - 5.606673 89950 - 8.507503 -1.99900 -17.920003

TABLE (2.08)

LIFT AND MOMENT COMPTICIENTS COMPUTED FROM DIETZE

ω	Mp	Lp	Th
.5	- 2.7949942520j	- 2.88932 + 1.15560j	+ .04516038801
-4	- 4.1973965562j	- 4.78622 + 1.90688j	+ .04216045625
.3	- 7.15183 - 1.05489j	- 9.18150 + 3.70666j	+ .03695059563
.2	-15.47739 - 1.83875j	- 23.24622 + 9.42250j	+ 0.02653 -0.092253
.1	-59.63739 - 4. 63400j	-115.34372 + 40.23000j	00472 .20800j

ω	Ta	Tp	
.5	0439920532j	17621091445	
.4	08201245563	2697211350j	
.3	1700630722j	4726314489j	
.2	- 0.44214 - 0.40850j	- 1.06466 - 0.18750j	
.1	- 2.099 39 54100j	- 4.3804120100j	

CONCLUSIONS

The method described in this report is suitable for the computation of compressible, non-stationary, aerodynamic lift and moment coefficients for values of the reduced frequency less than 1.

The subject method is better adapted to routine computation than are those previously known.

RECOMMENDATIONS

It is recommended that:

- 1. The results of this report be extended by the method described therein to cover a larger range of values of the control surface chord.
- 2. The accuracy of the linear approximation for the value .5 of the reduced frequency be checked using a cubic approximation for the nuclear difference.
- 3. Calculations be made using the cubic approximation for values of the reduced frequency between .5 and 1.0.

BIBLIOGRAPHY

- Kussner, H. G. and Schwartz, L. <u>Der Schwingende Flugel mit Aerodynamisch Ausgeglichenem Ruder</u>, Luftfahrt-Forschung, Vol. 17, Dec. 10, 1940, pp. 337-354. (Also available as NACA Tech. Memo. No. 991, 1941).
- Schwartz, L. Berechnung Der Druchverteilung Einer Harmonisch Sich Verformenden Tragfläche in Ebener Strömung, Luftfahrt-Forschung, Vol. 17, Dec. 10, 1940, pp. 379-386.
- Dietze, The Air Forces of the Harmonically Vibrating Wing in a Compressible Medium at Subsonic Velocity, Part I, AF Translation #F-TS-506RS, Aug. 9, 1946, and F-TS-948-RE, March, 1947; Part II, AF Translation #F-TS-948RE, March, 1947, and Chance Vought Report No. GTR-65, June 1947.
- Küssner, H. G. <u>Allgemeine Tragflächentheorie</u>, Luftfahrt-Forschung, Vol. 17, Dec. 10, 1940, pp. 370-378. (Also available as NACA Tech. Memo. No. 979).
- Frazer, R. A. and Skan, Sylvia <u>Influence of Compressibility on the Flexural</u>
 <u>Torsional Flutter of Tapered Cantilever Wings</u>, NPL Report No 5916.0.274, revised.
- 6 Cox, W. E. Possio's Compressibility Theory Applied to a Wing-Aileron Combination. Engineering Div. Memo. Report TSEAL2-4595-2-2, Nov. 24, 1945.
- 7 Smilg, Ben and Wasserman, Lee S. <u>Application of Three Dimensional Flutter</u>
 <u>Theory to Aircraft Structures</u>, AF Technical Report No. 4798, July 9, 1942.
- 8 Miles, J. W. A Note on a Solution to Possio's Integral Equation for an Oscillating Airfoil in Subsonic Flow, Quarterly of Applied Mathematics, Vol. VII, No. 2, July 1949.
- 9 Haskind, M. D. Oscillation of a Wing in Subsonic Gas Flow, Applied Mathematics and Mechanics, Vol. II, March 8, 1947, pp. 128-147.
- Timman R. and Van de Vooren, A. I. <u>Theory of the Oscillating Wing with Aerodynamically Balanced Control Surface in a Two-Dimensional.</u> Subsonic. Compressible Flow, Report No. F-54, Amsterdam Nationaal Luchtvaart Laboratorium.
- Possio, C. The Air Forces on Oscillating Frofile in a Compressible Fluid at Subsonic Speeds, Aerotechnica, Vol. 18, No. 4, 1938.
- Schade, Numerical Solution of the Possio Integral Equation of the Vibrating Wing in Plane Subsonic Flow, Fart I, Curtiss Wright Report No. U-19, September 30, 1946; Part II, AF Translation No. F-TS-987-RE, March, 1947

- Eichler, M. Auflosung Der Integral Gleichung Von Possio, FB No., 1681, Dessau 1942.
- Janke & Ende, Tables of Functions, Fourth Edition, Dover, 1945.
- 15 Whittaker & Watson, Modern Analysis, Macmillan, 1943
- Schwartz, Tables for the Calculation of the Air Forces of the Wibrating Wing in Compressible Two Dimensional Subsonic Flow. AF Trans. No. F-TS-599-RE, July 1946.
- 17 Inke, Y. L. Tables of Coefficients for Compressible Flutter Calculations. AF TR No. 6200.

APPENDIX I

EVALUATION OF CERTAIN INTEGRALS

A. Froof of Equation (1.13)

The relation as stated in equation (1.13) is

(A1.01)
$$\int_{1-z}^{1/2} dz \int_{z-z}^{z} \frac{\pi(z)dz}{z-z} = \pi \int_{z_1}^{z} \pi(z)dz$$

Schwartz (Ref. 2) has established the validity of the intercharge of the order of integration in the double integral above, and other integrals of this type; thus

(A1.02)
$$\int_{1/2}^{1/2} dz \int_{1/2}^{1/2} \frac{dz}{z-\xi} dz = \int_{1/2}^{1/2} \frac{dz}{z-\xi}$$
Now
$$\int_{1/2}^{1/2} \frac{dz}{z-\xi}$$
 becomes upon setting $z = \cos \theta$, $\xi = \cos \theta$
(A1.03)
$$\int_{1/2}^{1/2} \frac{dz}{z-\xi} = \int_{1/2}^{1/2} \frac{dz}{z-\xi} dz = (1+\cos \theta) \int_{1/2}^{1/2} \frac{dz}{z-\xi} dz$$

The above integral is of the Cauchy "principal-value" type, and it is well known that

$$(A1.04) \qquad \int_{\cos \varphi - \cos \theta}^{\pi} = 0$$

Thus

(A1.05)
$$\int \frac{1+2}{1-2} dz \int \frac{\pi(z)dz}{z-z} = \pi \int \pi(z)dz$$

B. Proof of Equation (1.14)

The relation to be proved is

(A1.06)
$$= \int_{-\pi}^{\pi} \int_{-\pi}^{\pi}$$

Designating the right side by u(x). then since (Ref. 2, Equation 62)

(A1.07)
$$\frac{d}{dx} \Lambda(x,z) = \sqrt{\frac{1+z}{1-z}} \left\{ \sqrt{\frac{1-x}{1+x}} \frac{1}{z-x} - \frac{1}{\sqrt{1-x^2}} \right\}$$

(A1.08)
$$\pi \frac{du}{dx} = \sqrt{\frac{1-x}{1+x}} \sqrt{\frac{1+z}{1-z}} \frac{dz}{z-x} / \frac{\pi(z)dz}{z-z} \sqrt{\frac{1}{1-z^2}} \sqrt{\frac{1+z}{1-z}} dz / \frac{\pi(z)dz}{z-z}$$

By equations (1.11) and (A1.05)

(A1.09)
$$\frac{du}{dx} = \pi \left[II(x) - \frac{1}{\sqrt{1-x^2}} \right] II(\xi) d\xi$$

Further A(l, 2) = 0 so that U(l) = 0. Therefore

(A1.10)
$$u(x) = \int \frac{dz}{\sqrt{1-z^2}} \left(\int \underline{\pi}(z) dz \right) - \pi \int \underline{\pi}(z) dz$$

OT

(A1.11)
$$\pi \int \Lambda(x,z) dz \int \frac{\pi(z)dz}{Z-i} = \cos^2 z \int \pi(z)di - \pi \int \pi(z)dz$$

C. Evaluation of the integral
$$\sqrt{\frac{1-\xi}{1+\xi}}e^{-\frac{2}{3}k\xi}d\xi$$

Set Y=cose, X=cose Ther

(A1.12)
$$\int \frac{1-\xi}{1+\xi} e^{-i\mu\xi} d\xi = \int (1-\cos\varphi) e^{-c\mu\cos\varphi} d\varphi$$

The function

is designated by $\int_{\mathcal{A}} (A_0)$. Properties of this function are discussed further in Appendix IV. Thus

For x^{2-i} , since $\int_{a}^{b} (u, \pi) = \pi(i)^{n} \int_{a}^{b} (u)$, this gives

(A1.144)
$$\int \int \frac{1-\xi}{1+\xi} e^{-i\mu\xi} d\xi = \pi \left[\int_{0}^{\infty} (\mu) + i \int_{0}^{\infty} (\mu) \right]$$
D. Evaluation of the integral
$$\int_{0}^{\infty} e^{-i\mu\xi} d\xi$$

Making the change of variables: 2 = cos 4, X= cos 6,

(A1.15)
$$\int_{\mathcal{R}} e^{-\xi \mathbf{A} \mathbf{E}} dt = \int_{0}^{0} e^{-\xi \mathbf{A} \mathbf{C} \cdot \mathbf{S} \mathbf{Q}} \sin \theta \, d\theta$$

Integrating by parts, with

whence

(A1.16)
$$\int_{C} e^{-i\mu \cos \theta} \sin \theta d\theta d\theta = \frac{1}{\sin \theta} \left[\theta e^{-i\mu \cos \theta} - \int_{C} e^{-i\mu \cos \theta} d\theta \right]$$

and for x=-/

(A1.18) in
$$e^{-i\mu k}$$
 cost de = $\pi[e^{i\mu}J_{o}(\mu)]$.

E. Evaluation of the integral

By the usual change of variables,

$$\int_{\mathcal{I}} \sqrt{1-\xi^{2}} e^{-\xi R\xi} d\xi = \int_{\mathcal{I}} e^{-\xi R\xi} d\xi = \int_{\mathcal{I}} e^{-\xi R\xi} d\xi d\xi$$

$$= \frac{1}{2} \int_{\mathcal{I}} e^{-\xi R\xi} d\xi = \int_{\mathcal{I}} e^{-\xi R\xi} d\xi d\xi$$

$$= \frac{1}{2} \left[\int_{\mathcal{I}} (2R, \theta) - \int_{\mathcal{I}} \xi R, \theta \right]$$

But equation (A4.07)

Therefore,

(A1.20)
$$\int_{z}^{1-z^{2}} e^{-i\alpha z} dz = i \int_{z}^{1} (\gamma u_{1} \cos^{2} z) - e^{-i\alpha z} \sqrt{1-z^{2}}$$

and for Xa-

(A1.21)
$$\int_{I-\xi^2}^{\iota} e^{-\epsilon x} dz = I J_i(x)$$

F. Evaluation of the integral \\ \(\frac{2\sqrt{1-\frac{1}{2}}}{2\sqrt{1-\frac{1}{2}}} \)

(A1.22)
$$\int_{2}^{1} E \sqrt{1-E^{2}} e^{-GA} dz = \int_{0}^{0} e^{-GA} \cos \theta \sin \theta \cos \theta d\theta$$

Integrating by parts with

gives

(A1.23)
$$\int_{0}^{\theta} e^{-\frac{i}{2}\alpha \cos \theta} \sin^{2}\theta \cos \theta d\theta = \frac{1}{i\mu} \left[e^{-\frac{i}{2}\alpha \cos \theta} \sin \theta \cos \theta - \int_{0}^{\theta} e^{-\frac{i}{2}\alpha \cos \theta} \cos \theta d\theta \right]$$
$$= \frac{1}{i\mu} \left[e^{-\frac{i}{2}\alpha \cos \theta} \cos \theta - \int_{2}^{\theta} (-\alpha, \theta) \right]$$

Therefore

(11.24)
$$\int_{2}^{1} \xi \sqrt{1-\xi^{2}} e^{-i\mu \xi} d\xi = \frac{i}{\pi} \left[\int_{2}^{1} (\gamma u, \cos \chi) - \chi \sqrt{1-\chi^{2}} e^{-i\mu \chi} \right]$$

and if x = -1

(A1.25)
$$\int_{\mathcal{L}} \mathcal{L}_{I-\underline{L}^2} e^{-i\lambda_{\underline{L}}} dt = -\frac{i\pi}{\mu} J_2(\mu)$$

TABLE (A1.01)

VALUES OF POINT 1+ E de

ω	χ=e = . 5
-0 .05 .10 .20 .30 .40	.1811722-01 .181067800604781 .180754201208831 .179502702411681 .177424103602641 .174529104775821 .170833805925471

VALUES OF IMPERIOR de

ω	x=e=.5
.05 .10 .20 .30 .40	.0 .000552+.0164401 .002206+.0328231 .008801+.0651881 .019721+.0966381 .034855+.1207281 .054053+.1550221

TABLE (A1.03)
VALUES OF Period (1-23 d)

W	z.e5
.0 .05 .10 .20 .30 .40	.3070925 0 .306910201039861 .306363702078401 .304181204146251 .300557206193071 .295511508208511 .289069510182261

VALUES OF SE TIPE ZELZ

ထ	Z=l=.5
.0. .05 .10 .20 .30 .40	.2165064-01 .216367100758761 .215958001516421 .214312603024271 .211581804516161 .207779105983931 .202921607418731

APPENDIX II

EVALUATION OF
$$\int_{x}^{e^{-i\mu \xi}} \bar{q}_{m}(t) dt$$
, $\int_{x}^{e^{-i\mu \xi}} \bar{q}_{m}(t) dt$

By definition equation (1.18)

(A2.01)
$$\Phi_m(x) = \int_{C} G(x,Z)u_m(z)dz$$
, $m = 0,1,--- m$.

According to Küssner (Ref. 1), this expression may be written as

(A2.02)
$$\Phi_m \left(-\cos\theta\right) = -2\left[q_0^m \left(\frac{1+\cos\theta}{\sin\theta}\right) + 2\sum_{k=1}^{m+1} q_k^m \sin k\theta\right]$$

with 2 = -coso, where

(A2.03)
$$Q_{n}^{m} = \frac{1+\Gamma(\omega)}{2} \left[P_{n}^{m} - P_{n}^{m} \right] - P_{n}^{m}, + > 0$$

and
$$U_{\infty}(z)[z=-\cos \varphi]$$
 has the form

(A2.04)
$$U_m(-\cos\phi) = P_o^m + 2 \sum_{n=1}^{n-m} P_n^m \cos n \phi$$

Expressions for the F's in terms of the coefficients \mathcal{C} may be found by converting the powers of $\cos \varphi$ into cosines of multiples of φ . For m=3,

$$P_{0}^{2} = \alpha_{0} + \omega^{2} \alpha_{2}, P_{1}^{2} = -\omega \alpha_{1} - 3\omega^{3} \alpha_{3}, P_{2}^{2} = \omega^{3} \alpha_{4}, P_{3}^{2} = -\omega^{3} \alpha_{5}, P_{1}^{2} = -\omega^{2} \alpha_{4}, P_{2}^{2} = -\frac{3\omega^{3} \alpha_{5}}{2}$$

$$(A2.05)$$

$$P_{0}^{2} = \omega^{2} \alpha_{2}, P_{1}^{2} = \frac{3\omega^{3} \alpha_{5}}{2}$$

$$P_{0}^{3} = -\omega^{3} \alpha_{5}$$
WADC TR 52-56

Finally,
$$\int_{\mathcal{X}} e^{-i\mu k} d\mu_{m}(k) dk = \int_{0}^{\infty} e^{-i\mu \cos k} d\mu_{m}(\cos k) \sin k d\mu_{m}, \quad x = \cos k$$

$$= -2 \int_{0}^{\infty} e^{-i\mu \cos k} \left\{ \left[a_{0}^{m} + a_{1}^{m} \right] - \left[a_{0}^{m} + a_{2}^{m} \right] \cos k + \left[a_{3}^{m} - a_{1}^{m} \right] \cos k \phi \right\} d\mu_{m}(k) dk = \int_{0}^{\infty} e^{-i\mu k} d\mu_{m}(k) d\mu_{m}(k) dk = \int_{0}^{\infty} e^{-i\mu k} d\mu_{m}(k) d\mu$$

Since $\int_{0}^{\theta} e^{-i\mu \cos \theta} \cos \eta d\eta = \int_{n}^{\infty} (-\mu, \theta)$, and since by equation (A4.07)

(A2.07)
$$\int_{n-1}^{\infty} (-\mu, \theta) - \int_{n+1}^{\infty} (-\mu, \theta) = \frac{2in}{n} \int_{n}^{\infty} (-\mu, \theta) - \frac{2i}{n!} e^{i\pi n} e^{i\pi n} \theta$$

it follows that

$$\int_{2}^{1-i\mu\xi} e^{-i\mu\xi} d\mu(\xi) d\xi = -2 \left\{ a_{0}^{m} \left[j_{0}(\mu,\theta) - j_{\mu}(-\mu,\theta) \right] - \frac{2i}{\mu} \sum_{n=1}^{m-m+1} (-)^{n} n a_{\mu}^{m} j_{n}(-\mu,\theta) + \frac{2i}{\mu} e^{-i\mu\xi \cos\theta} \sum_{n=1}^{m-m+1} (-)^{n} a_{\mu}^{m} \sin n\theta \right\}, m=0,1,2,-(n+m)$$

For Z=-/ this gives

$$(42.09) \int_{-1}^{1-2u\xi} d_{m}(\xi) d\xi = -2\pi \left\{ a_{0}^{m} \left[J_{0}(u) + i J_{i}(u) \right] - 2i \sum_{k=1}^{n-m+1} (i)^{k} R a_{k}^{m} J_{k}(u) \right\}$$

If M = 0 we obtain

$$(A2.10) \int q_{m}(\xi) d\xi = -2 \left\{ \theta \left[a_{0}^{m} + a_{1}^{m} \right] - \sin \left[a_{2}^{m} + a_{0}^{m} \right] + \frac{\sin 2\theta}{2} \left[a_{3}^{m} - a_{1}^{m} \right] - \cdots \right\},$$

$$(\chi = \cos 0)$$

and for M=0, X=-/ [0=1]

Similarly,

(A2.12)
$$\int_{-1}^{1} q_{m}(t) t dt = \pi \left[a_{o}^{m} + a_{x}^{m} \right], \int_{-1}^{1} q_{m}(t) t dt = -\pi \left[a_{o}^{m} + \frac{1}{2} \left(a_{i}^{m} + a_{x}^{m} \right) \right], \text{ et c.}$$

APPENDIX III

EVALUATION OF
$$B_0(x) = \int_{x}^{e^{-i\mu x}} e^{-i\mu x} dx dx = \int_{x}^{e^{-i\mu x}} E^{-i\mu x} dx$$

For practical purposes the above integrals must be evaluated for four types of motions, these are:

1. Translation of the entire chord.

2. Rotation of the entire chord about the forward quarterchord point.

3. Translation of the control surface.

4. Rotation of the control surface.

It has been shown by Küssner (Ref. 1) that in each of the first two cases, the pressure distribution ______() is expressible in the form

where A is the non-dimensional amplitude of the motion and the Gare functions only of the reduced frequency, as given in Table A.3.01. Thus the evaluation of \(\begin{align*} \text{C} & \text{TL}_0 (\beta) & \text{T} & \text{is in these cases reduced to the determination of the integrals} \end{align*}

These have already been shown in Appendix I to be respectively

$$\int_{x}^{-i\mu\xi} \frac{1-\xi}{1+\xi} d\xi = j_{0}(-\mu, \cos^{2}x) - j_{1}(-\mu, \cos^{2}x)$$

$$(A3.03) \int_{x}^{-i\mu\xi} \frac{1-\xi^{2}}{1-\xi^{2}} d\xi = \frac{i}{\mu} \left[j_{1}(-\mu, \cos^{2}x) - e^{-i\mu\chi} \int_{1-\chi^{2}}^{1-\chi^{2}} \right]$$

$$\int_{x}^{-i\mu\xi} \frac{1-\xi^{2}}{\xi} d\xi = \frac{i}{\mu} \left[j_{2}(-\mu, \cos^{2}x) - e^{-i\mu\chi} \right]$$

In the last two cases the incompressible pressure distribution consists of terms of the above type and additional terms of the form

(A3.04)
$$R_{p}(\xi-e)^{p}\Lambda(\xi,e)$$
, $p=0,1,2,$

where e is the coordinate of the control surface leading edge. The integral

(A3.05)
$$I_{\mu}(u, x, e) = \int_{x}^{e^{-i\mu x}} (z-e)^{\mu} \Lambda(z, e) dz$$

is discussed in Appendix V. Thus the general expressions for \mathcal{B}_o become as follows:

$$\frac{1}{\sqrt{1-\lambda^{2}}}B_{0}(x) = \frac{\pi\rho v^{2}b^{2}}{\sqrt{1-\lambda^{2}}}Ae^{ivt}\left\{\frac{Q_{1}(\omega,e)}{\pi}\left[j_{0}(-\mu,\cos^{2}x)-j_{1}(-\mu,\cos^{2}x)\right]\right. \\
+\frac{i}{\mu}\frac{Q_{2}(\omega,e)}{\pi}\left[j_{1}(-\mu,\cos^{2}x)-e^{-i\mu x}\sqrt{1-x^{2}}\right] \\
+\frac{i}{\mu}\frac{Q_{3}(\omega,e)}{\pi}\left[j_{2}(-\mu,\cos^{2}x)-e^{-i\mu x}\sqrt{1-x^{2}}\right] \\
+\frac{R_{0}}{\pi}T_{0}(\mu,x,e)+\frac{R_{1}}{\pi}T_{1}(\mu,x,e)+\frac{R_{2}}{\pi}T_{2}(\mu,x,e)\right\}$$

$$\frac{1}{\sqrt{1-\lambda^{2}}}B_{o}(-1) = \frac{\pi\rho\gamma^{2}b^{2}}{\sqrt{1-\lambda^{2}}}Ae^{-i\gamma^{2}}\left\{Q_{1}\left[J_{o}(M)+iJ_{1}(M)\right]+Q_{2}\left[J_{1}(M)/M\right]\right.$$

$$+Q_{3}\left[\frac{-iJ_{1}(M)}{M}\right] + \frac{R_{0}J_{o}(A,-1,e)}{M}J_{1}(A,-1,e) + \frac{R_{1}J_{1}(A,-1,e)}{M}J_{1}(A,-1,e)\right\}$$

where the Q; and R; are listed in Table A (3.01) for the four types of motion to be considered.

It is noted that for airfoils with a single control surface it is necessary to consider only the case where x = e.

The integrals
$$B(\epsilon) = \int_{\epsilon} Z_{\delta}(\epsilon) d\epsilon$$
, $B_{\delta}(\epsilon) = \int_{\epsilon} Z_{\delta}(\epsilon) \epsilon d\epsilon$ are

already known, being respectively the incompressible lift over the portion of the airfoil extending from x= e to x= 1, and the total incompressible moment about the midchord. In the notation of Reference 6, these are:

(1)
$$B_{i}(e) = \pi \rho v^{2} b^{3}(h_{i}) P_{k}(e)$$
, $B_{i}(-1) = \pi \rho v^{3} b^{3}(h_{i}) L_{k}$
(2) $B_{i}(e) = \pi \rho v^{3} b^{3} \alpha_{o} P_{\alpha}(e)$, $B_{i}(-1) = \pi \rho v^{3} b^{3} \alpha_{o} L_{\alpha}$
(3) $B_{i}(e) = \pi \rho v^{3} b^{3}(2 \gamma_{b}) P_{2}(e)$, $B_{i}(-1) = \pi \rho v^{3} b^{3}(2 \gamma_{b}) L_{2}$
(4) $B_{i}(e) = \pi \rho v^{3} b^{3} \rho_{o} P_{\rho}(e)$, $B_{i}(-1) = \pi \rho v^{3} b^{3} \rho_{o} L_{\rho}$

(80.EA)

(1)
$$B_{2}(-1) = \pi \rho v^{2} b^{4}(h_{0/b}) [M_{h} - \frac{1}{2} L_{h}]$$

(2) $B_{2}(-1) = \pi \rho v^{2} b^{4} d_{0} [M_{K} - \frac{1}{2} L_{K}]$
(3) $B_{2}(-1) = \pi \rho v^{2} b^{4} (\frac{2}{9}) [M_{2} - \frac{1}{2} L_{2}]$
(4) $B_{2}(-1) = \pi \rho v^{2} b^{4} \rho_{0} [M_{p} - \frac{1}{2} L_{p}]$

The relations (A3.08) are useful as checks on the computation of $\mathcal{B}_{o}(x)$ since $\mathcal{B}_{o}(x) = \lim_{N \to 0} \mathcal{B}_{o}(N, x)$

For the evaluation of $\mathcal{B}_{\mathbf{3}}$ the following integrals are needed:

$$\int \sqrt{\frac{1-\ell}{1+\ell}} e^{2} de , \int \sqrt{1-\epsilon^{2}} e^{2} de , \int \sqrt{1-\epsilon^{2}} e^{2} de$$

$$\int \Lambda(\ell,e) e^{2} de , \int \Lambda(\ell,e) (\ell-e) e^{2} de , \int \Lambda(\ell,e) (\ell-e)^{2} e^{2} de$$

These are found to be respectively:

$$\int_{-1}^{1-\epsilon} \frac{1-\epsilon}{1+\epsilon} \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} \frac{1-\epsilon^{2}}{1+\epsilon} \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} \frac{1-\epsilon^{2}}{1+\epsilon} \epsilon^{2} d\epsilon = 0$$
(A3.09)
$$\int_{-1}^{1} \Lambda(\epsilon,e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} \Lambda(\epsilon,e) (\epsilon-e) \epsilon^{2} d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon+2e^{2}) d\epsilon = \pi/2 \qquad \int_{-1}^{1-\epsilon^{2}} (\epsilon$$

(A3.10)
$$B_3 = \pi \rho b^3 v / 1 \left\{ \frac{1}{2} Q_1 + \frac{1}{8} Q_2 + \frac{1}{6} R_0 \sqrt{1 - e^2} (1 + 2e^2) - \frac{1}{24} R_1 \sqrt{1 - e^2} (2 + 2e^3) + \frac{1}{120} R_2 \sqrt{1 - e^2} (9 + 2e^3 + 4e^4) \right\}$$

Mode of Motion	õ	42	ර්	Ro	Я,	Rx
Translation of	$-\frac{i}{\omega}\left\{ + 7(\omega) \right\}$	7	0	0	0	٥
Rotation about	$-\left\{\frac{1+T(\omega)}{\omega^4}+\frac{iT(\omega)}{\omega}\right\}$	1 - 4·¿	/	0	0	0
1	$\frac{i}{\pi} \left\{ \frac{24i - e^{\pm}}{\omega} - \left[\frac{i + 7(\omega)}{\omega} \right] \underline{\Phi}_i(e) \right\}$	2 cos-'e	0	726	46	0
Rotation of	1 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1 / 1-ex-# cose-zecore	1 Cos'e		7 2 2	<u>'</u> π
Coefficients:						
For Bo	$J_o(\mu) + i J_o(\mu)$	J,(42)/4	-i Ja (4)/4	1 To (4,-4)	(a'-'a)'I#	-: Ja (4)/4 1/2 (4,-10) 1/2 (4,-10) 1/2 (4,-10)
For $\pi \mathcal{B}(\kappa)$	/ (-4, cos"x) - / (-4, cos"x)	1/4, co o'x -e that first	in { i, (-a, cost cos	I, (A, C, E)	I, (4.c.e)	$\frac{i}{\mu} \left\{ i_j(\mathcal{A}, \omega_s^* \mathbf{x}) \right\} \mathcal{I}_{\sigma}(\mathbf{A}, e, e) \mathcal{I}_{\sigma}(\mathbf{A}, e, e)$ $-\tilde{e}^{i_j \mathbf{x}} \mathbf{x}_{J_{\tau} \cdot \mathbf{x}^* \mathbf{x}}$
For B ₃ :	-1/2	1/8	0	1-6- [1-26]	1.c. (e.26)	11-ex (1-20) 11-ex (11-ex (5-20 20) (120)

The quantities $\Phi_{\ell}(e)$, $\Phi_{2}(e)$, $\Phi_{3}(e)$ are defined by Kussner in Ref. 1, and are not related to the function $\Phi_{n}(x)$ defined by equation 1.18. The function T(e) is related to C(e) according to equation 1.08.

APPENDIX IV

THE FUNCTION JAMES

By definition

(44.01)

a. Special Values -

The function is seen to possess the following limiting

values:

(A4.02)

$$\int_{\mathcal{D}} (u,\pi) = \pi(i)^n \mathcal{J}_n(u) \quad ;$$

(44.03)

$$J_n(u, T_2) = \frac{\pi}{2} e^{in\frac{\pi}{2}} [J_n(u) - i E_n(u)],$$

where E_n is the Lommel-Weber function of order π ;

(A4.04)

b. Differential Relations -

By differentiation of equation (A4.01)

$$\frac{\partial}{\partial \mu} \left[j_n(\mu, \theta) \right] = i \int_0^{\theta} e^{i\mu \cos \theta} \cos \theta \, d\theta \, d\theta$$

$$= \frac{i}{\lambda} \int_0^{\theta} e^{i\mu \cos \theta} \left[\cos (\pi n) \, \theta + \cos (\pi n) \, \theta \right] \, d\theta \, .$$

Or,

$$\frac{\partial}{\partial u} \left[\int_{\mathcal{H}} (u, \theta) \right] = \frac{\partial}{\partial u} \left[\int_{\mathcal{H}_{1}} (A, \theta) + \int_{\mathcal{H}_{2}} (A, \theta) \right]$$

In particular, for n = 0,

$$(A4.06) \qquad \frac{\partial}{\partial x} \left[J_0 \left(A, \Theta \right) \right] = \tilde{i} J_1 \left(A, \Theta \right)$$

c. Recurrence Formulae -

Integration of Equation (A4.01) by parts gives

(A4.07)

or

(A4.08)
$$\int_{M+1} (A, \theta) = \frac{2i\pi}{M} \int_{P_{\epsilon}} (A, \theta) + \int_{R-1} (A, \theta) - \frac{2i}{M} e^{-i\mu \cos \theta} \sin(\pi \theta)$$

d. The Differential Equation Satisfied By $\int_{\mathcal{H}} (u, e)$ Differentiation of (A4.05), together with successive applications of equations (A4.05), together with successive applications of equations (A4.05) and (A4.08), shows that $\mathcal{L}(u, e)$ satisfies the differential equations

(M.09)
$$\frac{d^{2}y}{d\mu^{2}} + \frac{1}{n} \frac{dy}{dn} + \left[1 - \frac{n^{2}}{n^{2}}\right] y = e^{\frac{1}{2}n\cos(n\theta)} \int_{\mathbb{R}^{2}}^{\infty} \cos(n\theta) \sin(n\theta) d\theta$$

In particular, (4,0) is a solution of

e. Expansion of J. (A.O.) and J. (A.O.) as Power

Series in cos P

It has already been shown that $\int_{\theta} (A, \theta)$ is a solution of the equation

(84.11)
$$A \frac{d^{4}x}{d\mu} + \frac{d^{4}x}{d\mu} + \mu \dot{y} = i e^{i h \cos \theta}$$

$$= i \sin \theta \sum_{h=0}^{\infty} \frac{(i h \cos \theta)^{h}}{h!}$$

It follows that John) can be written in the form

where Age eatisties the equation

and it is easily shown that a solution of this equation is

(M.14)
$$A_{R}^{\prime}(u) = \frac{M^{2}}{(R+1)^{2}} \left[1 - \frac{M^{2}}{(R+3)^{2}} + \frac{M^{4}}{(R+3)^{2}(A+5)^{2}} + \dots \right]$$

The Az satisfies the recurrence relation

with the following initial values

(A4.16)
$$A_o(x) = -\frac{\pi}{2} E_o(x)$$

 $A_i(x) = 1 - J_o(x)$

where E is the Weber function of order zero.

As a check on the computation of the A's, the following relations are useful:

$$\left(\begin{array}{c}
 A_{1}(A) - \frac{A_{3}(A)}{3!} + \frac{A_{5}(A)}{5!} = J_{0}(A) - \cos(\mu) \\
 A_{0}(A) - \frac{A_{2}(A)}{2!} + \frac{A_{4}(A)}{4!} = \sin(A)
 \end{array} \right)$$
HADO TR 52-56

Further, since $I_{Q}(0,\theta) = \theta$ and $A_{R}(0) = 0$, it follows that B = 0 and $A = \theta$ in Equation (A4.12). Thus, finally

Separating real and imaginary parts,

$$(A4.19) \begin{cases} \int_{0}^{\pi} (A, \theta) = \theta J_{0}(A) - \sin \theta \sum_{R=0}^{\infty} (-)^{R} A_{R^{(1)}}(A) \frac{\cos^{2R+1}\theta}{(2R+1)!} \\ \int_{0}^{\pi} (A, \theta) = \sin \theta \sum_{R=0}^{\infty} (-)^{R} A_{R^{(1)}}(A) \frac{\cos^{2R}\theta}{(2R)!} \end{cases}$$
Since
$$\int_{0}^{\pi} (A, \theta) = -i \frac{d}{dA} \int_{0}^{\pi} (A, \theta)$$

$$\int_{IR} (\mu, \theta) = \sin \theta \sum_{R=0}^{\infty} (-1)^{R} B_{2R}(\mu) \frac{\cos^{2R} \theta}{(2R)!}$$

$$\int_{IR} (\mu, \theta) = \theta \int_{IR} (\mu) + \sin \theta \sum_{R=0}^{\infty} (-1)^{R} B_{2R+1}(\mu) \frac{\cos^{2R+1} \theta}{(2R+1)!}$$

where

For n>1, $f(A, \theta)$ may be found from the relation

(A4.22)
$$\int_{N+1} (A, \theta) = \frac{26\pi}{n} \int_{R} (A, \theta) + \int_{N+1} (A, \theta) - \frac{26}{n} C \int_{R} C \int_{R}$$

However, if $A \le l$, this formula may be subject to considerable error unless the lower order functions are carried to many more places than is required in the final results. In such cases it may be preferable to employ the following type of expansions obtained by applying Equation (44.05). Thus for $f_{2}(A, \theta)$

(A4.23)
$$J_2(M,0) = \theta \left[J_0(M) - J_1(M) \right] - j_0(M,0) - 2i \sin \theta \sum_{n=0}^{\infty} (i)^n C_n(n) \frac{\cos^{\frac{n}{2}}\theta}{n!}$$
 with

$$(44.24) C_{R}(a) = \frac{d}{da} \left[B_{R}(a) \right] = \left[\frac{\pi}{\pi^{+1}} \frac{A^{-1}}{(R+1)^{2}(R+3)} \frac{\pi^{+1}}{(R+1)^{2}(R+3)^{2}(R+3)^{2}(R+3)^{2}(R+3)^{2}} \frac{\pi^{+3}}{(R+1)^{2}(R+3)^{2}(R+3)^{2}(R+3)^{2}} \right]$$

Similarly,

$$(M.25)$$
 $\int_{3} (M,8) = i \theta [3J,(n)-J_{3}(n)]-3J,(M,8)-4 sin \theta \sum_{n=0}^{\infty} (i) D_{n}(n) \frac{\cos^{n}\theta}{n!}$

with

(14.26)
$$D_{R}(u) = \frac{d}{du} \left[C_{R}(u) \right] = \left[\frac{R(R-1)}{(R+1)} u - \frac{(R+2)}{(R+1)(R+3)} u + \frac{R+4}{(R+1)^{2}(R+3)(R+5)} u \right]$$

TABLE (A4.01)

VALUES OF $\int_{\mathcal{H}}^{\infty} f dt$, $\cos^2 x$) $\lambda = .7$, $M = \frac{\lambda^2 \omega}{1 - \lambda^2}$

ω	n=0, x = .5		n=1,	Z = . S
.0	1.0471976 -	oi	.8660254	- oi
.05	1.0463437	0,159111	.8652759	03554331
.16	1.0437836	08311041	.8630294	0710221i
.20	1.0335647	16564581	.8540640	14152901
.30	1.0166208	.24703561	.8391967	21100921
.40	.9930688	32671781	.8185397	27895961
.50	.9630815	40414291	.79 22 47 7	34488821

ω	n=2, x=.5	7-1, Z=-5
.0	.4330127 - 0i	o - oi
.05	.432523302079391	000 1923 00519311
.10	.431056204154251	000802601336541
.20	.42520430 827 20 8 1	003186502055811
.30	.415506512317431	0071306 0303 630 1
.40	.40204 6 916254761	0125766039 6025 1
.50	.38494252004 9771	019438704813901

APPENDIX V

THE FUNCTION In (M, x, e)

a. Recurrence Relationships -

By definition

(A5.01)
$$I_n(x,z,e) = /e^{-\epsilon x \xi} (\xi - e)^n \Lambda(\xi,e) d\xi$$

whence

(A5.02)
$$\frac{d}{d\mu}\left[e^{i\mu e}I_{n}\right]=-i\int_{e}^{e^{-i\mu(k-e)}}(z-e)\Lambda(z,e)dz$$

or

(A5.03)
$$\frac{d}{d\mu}\left(e^{i\mu e}I_{n}\right)=-ie^{i\mu e}I_{n+1}$$

b. Value of $I_{\alpha}(x,x,e)$

Setting $x=\cos\theta$, $e=\cos\epsilon$, $y=\cos\varphi$, in (A5.01), we have,

for n=0,

(A5.04)
$$e^{iA\cos\epsilon}T_0 = \int_0^{\theta} e^{i\mu(\cos\epsilon-\cos\rho)} \Lambda(q,\epsilon) \sin q dq$$

Since (Ref. 1),

$$\frac{d}{d\theta} \Lambda(\theta, \epsilon) = \frac{\sin \epsilon}{\cos \theta - \cos \epsilon}$$

integration of (A5.03) by parts gives

(A5.05)
$$e^{i\mu\epsilon\sigma_s e} = \frac{\Lambda(\rho,\epsilon)[e^{i\mu(\cos\epsilon-\cos\theta)}-1]}{i\mu} + \frac{\sin\epsilon}{i\mu} \int_{\rho}^{\theta} \frac{e^{-i\mu(\cos\rho-\cos\epsilon)}}{\cos\rho-\cos\epsilon} d\rho$$

Introducing the notation

(A5.06)
$$F'(N,\theta,E) = \int_{0}^{\theta} \frac{-i\mu(\cos\phi - \cos E)}{\cos\phi - \cos E} d\phi$$

gives

(A5.07) is
$$e^{i\mu\cos\epsilon}I_0(u,x,e)=\Lambda(\theta,\epsilon)[e^{i\mu(\cos\epsilon-\cos\theta)}-1]+\sin\epsilon F(u,\theta,\epsilon)$$

The function $f(x, e, \epsilon)$ is discussed further in Section 1. of this Appendix.

For the present it is sufficient to note that

(45.08)
$$\frac{\partial F}{\partial u} = i \int_{C}^{C} -i\mu(\cos\phi - \cos\epsilon) d\phi = i e^{i\mu(\cos\epsilon)} (-\mu, \sigma)$$

Thus since $f^{(0,0,\epsilon)} = 0$

(A5.09)
$$F'(\mu,\theta,\varepsilon) = i \int_{0}^{\mu} it\cos \varepsilon \cdot (-t,\theta) dt$$

c. Value of I (M, x,e)

By (A5.03),

But also from (A5.07) and (A5.08)

(A5.11)
$$\frac{d}{d\mu}$$
 [i $\mu e^{i\mu \cos \theta}$] = $i\Lambda(\theta, \epsilon)$ $e^{i\mu(\cos \epsilon - \cos \theta)}$ (cose-cos θ) + $\iota\sin \epsilon e^{i\mu\cos \epsilon}$.

Thus

(A5.12) in
$$C^{i\mu cose} I_{i} = C^{i\mu cose} I_{i} - (cose-cose) \Lambda(\theta, \epsilon) C^{i\mu (cose-cose)} - sine C^{i\mu cose} I_{i} - (cose-cose) \Lambda(\theta, \epsilon) C^{i\mu cose} I_{i} - I_{i} -$$

or

d. Value of $\mathcal{I}_{2}(u,x,e)$ Differentiation of (A5.12) gives

(A5.14)
$$\frac{d}{d\mu}\left[i\mu e^{i\mu\cos\delta}I_{i}\right]=\frac{d}{d\mu}\left[e^{i\cos\epsilon\cos\delta}I_{o}\right]-i\left(\cos\epsilon-\cos\theta\right)\Lambda(o,\epsilon)e^{i\mu\left(\cos\epsilon-\cos\theta\right)}$$

-is in Exast (1-4,0) + i sint e (4.036)
and, applying (A5.03)

(A5.15) ie
$$I_1 + i\mu[-ie^{iR\cos \delta}I_2] = -ie^{iR\cos \delta}I_1 + isinee^{iR\cos \delta}I_2$$

whence
$$(A5.16) \quad i\mu \in I_{Z} = 2e^{i\mu\cos\theta} I_{i} + (\cos\epsilon - \cos\theta)^{2} \Lambda(\theta, \epsilon)e^{i\mu(\cos\epsilon - \cos\theta)} + \sin\epsilon\cos\theta e^{i\mu\cos\theta} I_{i} - \sin\theta e^{i\mu\cos\theta} I_{$$

or

(A5.17) in
$$I_{2}(u,x,e) = 2I, (u,x,e) + (x-e)^{2}\Lambda(cos^{2}z,cos^{2}e)e^{-Gux}$$

e. Special Values -

For x = -1, $\theta = \pi$, $\Lambda(\theta, \epsilon) = 0$, and the following expressions result:

(A5.18)
$$\lim_{\lambda \to I_{0}} (A, \forall, e) = e^{-i\mu e} \sqrt{1-e^{2}} F^{2}(A, \pi, \cos^{2}e)$$

$$\lim_{\lambda \to I_{1}} (A, -1, e) = I_{0}(A, \forall, e) - \pi \sqrt{1-e^{2}} J_{0}(A)$$

$$\lim_{\lambda \to I_{2}} (A, -1, e) = 2I_{1}(A, -1, e) + \pi e \sqrt{1-e^{2}} J_{0}(A) + i\pi \sqrt{1-e^{2}} J_{1}(A)$$
and for $B = e$, since $\lim_{\lambda \to e} (\cos \theta - \cos \epsilon) \Lambda(\theta, \epsilon) = 0$

$$\lim_{\lambda \to I_{0}} (A, e, e) = e^{-c\mu e} \sqrt{1-e^{2}} \int_{a}^{A} (A, \cos^{2}e, \cos^{2}e)$$

$$\lim_{\lambda \to I_{2}} (A, e, e) = I_{0}(A, e, e) - \sqrt{1-e^{2}} \int_{a}^{A} (-\mu, \cos^{2}e)$$

$$\lim_{\lambda \to I_{2}} (A, e, e) = 2I_{1}(A, e, e) + e \sqrt{1-e^{2}} \int_{a}^{A} (-\mu, \cos^{2}e)$$

$$\lim_{\lambda \to I_{2}} (A, e, e) = 2I_{1}(A, e, e) + e \sqrt{1-e^{2}} \int_{a}^{A} (-\mu, \cos^{2}e)$$

$$\lim_{\lambda \to I_{2}} (A, e, e) = 2I_{1}(A, e, e) + e \sqrt{1-e^{2}} \int_{a}^{A} (-\mu, \cos^{2}e)$$

WADC IR 52-56

52

The following limiting values may also be deduced:

f. Properties of the function $F'(u, e, \epsilon)$

It has already been noted (Equation A5.09) that

or

(A5.21)
$$F(u,\theta,\varepsilon) = -i \int_{0}^{\mu_{-i}t\cos\varepsilon} \int_{0}^{t} (t,\theta) dt$$

Now from Equation (A3.09)

$$\pm \frac{d^2 j_0}{dt^2} + \frac{d j_0}{dt} + t j_0 = i sono e^{ctcoso}$$

Multiplying both sides by C-CtCose

and integrating,

(A5.22)
$$\int_{e}^{M_{-c}t\cos\theta} \frac{dt}{dt} dt + \int_{e}^{M_{-c}t\cos\theta} \frac{dt}{dt} dt$$

$$+ \int_{e}^{M_{-c}t\cos\theta} \frac{dt}{dt} dt = i \sin\theta \int_{e}^{M_{c}t\cos\theta-\cos\theta} dt$$

The left side after several integrations by parts may be reduced to:

and the right side becomes

Sind
$$\left[\frac{e^{ip((cos\theta-cosb)}-1)}{(cos\theta-cosb)}\right]$$

But

(A5.23)
$$\frac{d}{d6} F(-A,0,6) = sine \begin{cases} A - iterse \\ f + dt \end{cases}$$

Thus

(45.24)

$$-i\mu e^{-i\mu\cos\theta} \left[\int_{I} + \cos\theta \int_{0}^{\pi} \right] + \sin\theta \left[\frac{e^{i\mu(\cos\theta - \cos\theta)} - 1}{\cos\theta - \cos\theta} \right]$$

or

$$\frac{d}{d\epsilon} \left[sin \epsilon \, f'(-\mu, \theta, \epsilon) \right] = sin \theta \left[\frac{e^{\mu (\cos \theta - \cos \epsilon)}}{\cos \theta - \cos \epsilon} \right]$$

(45.25)

Integrating,

Sine
$$F'(-\mu,0,\varepsilon) = \sin\theta / \frac{\varepsilon \omega(\cos\theta - \cos\theta)}{\cos\theta - \cos\theta} d\theta$$

(A5.26)

sin 8 F(4,6,0) - Sin 6 F(24,0,6)

(45.27)

- CA[[(M,0)](-A,0)+ [(-A,0)](M,0)]

If $\beta = \Pi$, this gives

or

and if $\theta = \epsilon$

Since $F(A, 6, \ell)$ and $F(-A, 6, \ell)$ are complex conjugates, the above relation gives only the imaginary part of F(A, 6, 6). Equations (A5.27) and (A5.30), while of little value for direct computation, are useful as numerical checks on results obtained from other methods.

g. Expansion of $\mathcal{F}(\mathcal{A},\theta,6)$ as a power series in \mathcal{K} .

By definition,

$$F(u,0,6) = \int \frac{1-e^{-iA(\cos\phi-\cos\delta)}}{\cos\phi-\cos\delta} d\phi$$

Expanding the numerator,

(A5.31)
$$F(A,0,\epsilon) = \int_{0}^{\infty} \frac{\left(-i\mu\right)^{R} \left(\cos\varphi - \cos\epsilon\right)^{R}}{R!} d\varphi$$

$$= -\sum_{0}^{\infty} \frac{\left(-i\mu\right)^{R}}{R!} \int_{0}^{\infty} \left(\cos\varphi - \cos\epsilon\right)^{R-1} d\varphi.$$

Then with the notation

(A5.32)
$$U_{h}(0, \epsilon) = \int_{0}^{0} (\cos \varphi - \cos \epsilon)^{\frac{1}{2}} d\varphi$$
, $h \ge 0$,
(A5.33) $F'(u, 0, \epsilon) = -\sum_{k=0}^{\infty} \frac{(\sin k)}{h!} U_{h}(0, \epsilon)$

The Un may be computed successively from the following recurrence relationship:

$$U_{R}(\theta, \epsilon) = \frac{\sin \theta}{R} \left[\cos \theta - \cos \epsilon\right]^{R-1} + \left(\frac{R-1}{R}\right) \sin^{2} \epsilon U_{R-2}(\theta, \epsilon) \\
- \left(\frac{2R-1}{R}\right) \cos \epsilon U_{R-1}(\theta, \epsilon), \qquad R \ge 2$$

starting with the initial values

(A5.35)
$$V_o(\theta, \epsilon) = \theta$$
, $V_i(\theta, \epsilon) = sen \theta - \theta \cos \epsilon$

In particular,

(A5.36)
$$U_{R}(\epsilon,\epsilon) = \left(\frac{R-1}{R}\right) \sin^{2}U_{R-2}(\epsilon,\epsilon) - \left(\frac{2R-1}{R}\right) \cos U_{R-1}(\epsilon,\epsilon)$$

with
$$U_{0}(\epsilon,\epsilon)=\epsilon$$
, $U_{1}(\epsilon,\epsilon)=\sin\epsilon-\epsilon\cos\epsilon$

Since
$$U_{h}(\sqrt[q]{2},\sqrt[q]{2}) = \int_{0}^{\pi/2} \cos^{n}\theta \, d\theta$$
 and since $\sum_{n=0}^{\infty} \cos^{n}\theta$ converges if $0<\theta<\pi/2$, so also does $\sum_{n=0}^{\infty} U_{h}(\sqrt[q]{2},\sqrt[q]{2})$, or, $\lim_{n\to\infty} U_{h}(\sqrt[q]{2},\sqrt[q]{2}) = 0$ Also, if $\leq <\pi/2$, $U_{h}(\varepsilon,\varepsilon) \leq U_{h}(\sqrt[q]{2},\sqrt[q]{2})$ Thus the series for $\sum_{n=0}^{\infty} U_{h}(\varepsilon,\varepsilon)$ converges more rapidly if $\leq <\pi/2$ since for $\leq >\pi/2$

$$U_{R}(\epsilon,\epsilon) \leq U_{R}(\pi,\pi) = 2^{R} \int_{0}^{\pi} \cos^{2R} \frac{d}{2} d\rho$$

and although the series $\sum \frac{(-i\lambda)^R}{R!} V_{R'}(\mathcal{E}, \mathcal{E})$ still converges, the convergence is poorer if $\pi/2 < \mathcal{E} < \pi$. In this case the following relation is useful:

(A5.37)
$$F'(\mu, \pi, \epsilon, \pi, \epsilon) = \frac{c\pi\mu}{5i\pi\epsilon} \left[J_0(\mu) \int_{\epsilon} (-\mu, \epsilon) + i J_1(\mu) \int_{\epsilon} (-\mu, \epsilon) \right]$$

 $+ F'(-\mu, \epsilon, \epsilon)$

TABLE (A5.01) - VALUES OF & F(M, x,e); e.s

w	7 =	e	x=-/	
0	1.0471976	-0	3.1415927	+01
.05	1.0471453	00822471	3.1406858	+.03771721
.10	1.0469886	01644781	3.1379702	+.07535831
.20	1.0463617	03288271	3.1271345	+.15010865
.30	1.0453176	04929191	3.1091812	+.22365061
.40	1.0438574	06566261	3.0842665	+,29539611

TABLE (A5.02) - VALUES OF Jo (A, x,e); e=.5

ω	% =	7=e 7=-/		-/
0.	.906899	- Oi	2,7206991	0i
.05	.9064218	02890091	2.7199140	03267031
.10	.9049887	05776911	2.7175606	06531241
.20	.8992647	11527591	2.7081584	13139871
.30	.8897558	17225991	2.6925324	19503421
.40	.8765085	22846291	2.6707474	25899641
.50	.8595872	28363111	2.6428903	32206481

TABLE (A5.03) - VALUES OF I, (4, 2, 2); e = .5

w	Z= E		72=	-1
0 .05 .10 .20 .30 .40	.148275 .1481707 .1478647 .1466385 .1446013 .1417670 .1381515	- 0i 00544561 0108828i 02169951 03239161 04289651 05315281	6801747 6800759 6797823 6786053 6766493 6739193 6704206	- 01 01633251 03264941 06513691 16009921 12902191 16009921

TABLE (A5.04) -VALUES OF In (u, 2, e); e = .5

ω	x= e		72-1	
0 .05 .10 .20 .30 .40	.0392250 .0391520 .0390673 .0387291 .0381164 .0372615 .0361732	- 01 00146801 00307551 00615881 00918211 01214941 01503541	.6801747 .6799926 .6791402 .6761256 .6710323 .6639488 .6549472	+ 0i +.0122171i +.0244863i +.0488642i +.0730556i +.0969448i +.12042491

AFP ANDIX VI

A DERIVATION OF THE INVERSION FORMULA FOR THE EQUATION $f(x) = \frac{1}{\pi} \int \frac{II(t) dt}{x-t}$

A. Special integrals -

In the following demonstration it is necessary to recall the following:

$$(A6.01) \qquad \int_{0}^{\infty} \frac{dq}{\cos q - \cos \varphi} = 0$$

where the symbol denotes the Cauchy principal value, i.e.

$$(46.02) \int \frac{dq}{\cos q - \cos \theta} = \lim_{\epsilon \to 0} \left\{ \int \frac{dq}{\cos q - \cos \theta} + \int \frac{dq}{\cos q - \cos \theta} \right\}$$

From this result it is easy to obtain by induction the following:

(A6.03A)
$$\int_{0}^{\pi} \frac{\cos(\pi\theta)d\theta}{\cos\theta - \cos\theta} = \pi \frac{\sin(\pi\theta)}{\sin\theta}$$

(A6.03B)
$$\int_{Cos - \cos \theta}^{\pi} \frac{\sin(\pi \theta) \sin \theta d\theta}{\cos \theta} = \pi \cos(\pi \theta)$$

B. Solution of the equation

The equation to be solved is

(A6.04)
$$f(x) = \frac{1}{\pi} \int_{-x}^{1} \frac{\pi(t) dt}{x - t}$$

Waking the substitution $\chi = \cos \theta$, $\mathcal{E} = \cos \theta$ in (A6.04)

(A6.05)
$$f(\cos \theta) = \frac{1}{\pi} \int \frac{\mathbf{E}(\cos \theta) \operatorname{sind} d\theta}{\cos \theta - \cos \theta}$$

WADC 52-56

Now assume a solution of (A6.05) of the form

(A6.06)
$$II(\cos \varphi) \sin \varphi = \sum_{n=0}^{\infty} a_n \cos(n\varphi).$$

Then with the aid of equation (A6.03A),

(A6.07)
$$sin \theta f(cos \theta) = \sum_{n=0}^{\infty} a_n sin(n\theta)$$

Multiplying both sides by $\left[\frac{\sin \theta}{\cos \theta - \cos \phi}\right]$ and integrating with respect to θ ,

(A6.08)
$$\int \frac{f(\cos\theta)\sin^2\theta d\theta}{\cos\theta - \cos\theta} = \sum_{n=0}^{\infty} \int \frac{\sin(n\theta)\sin\theta d\theta}{\cos\theta - \cos\theta}$$

Or, from (A6.03B)

(A6.09)
$$\int_{0}^{\pi} \frac{f(\cos \theta) \sin^{2}\theta d\theta}{\cos \theta - \cos \theta} = \pi \sum_{n=1}^{\infty} a_{n} \cos(n\theta)$$
$$= \pi \left[II(\cos \theta) \sin \theta - a_{0} \right]$$

Returning to the original variables x and Z,

(A6.10)
$$\int \frac{f(z)\sqrt{i-z^2} dz}{z-\varepsilon} = \pi \int II(\varepsilon)\sqrt{i-\varepsilon^2} - d_0$$

or, interchanging x and } !

(A6.11)
$$\sqrt{1-x^2} \, II(x) = a_0 - \frac{1}{\pi} / \frac{f(\epsilon) \sqrt{1-\epsilon^2} \, d\epsilon}{x-\epsilon}$$

It is noted that (A6.11) still contains the undetermined constant a_0 , the presence of which may be attributed to equation (A6.01) which renders this quantity arbitrary. Thus a_0 is analogous to a constant of integration in a differential equation and additional conditions must be imposed to determine it.

In this airfoil theory where equation (A6.04) relates the downwash f(x) to the pressure distribution $\mathcal{Z}(z)$, the Kutta condition requires that a finite pressure exist at the trailing edge, x = 1. It is clear from inspection of (A6.11) that the only value of a_0 for which this is possible is that one given by

(A6.12)
$$a_o = \frac{1}{\pi} \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} \frac{f(\xi)\sqrt{1-\xi^2}}{1-\xi} d\xi$$

Replacing so in equation (A6.11) by the above value and re-arranging gives

(A6.13)
$$II(x) = \frac{1}{II\sqrt{1+x}} \int_{-\frac{\pi}{2}}^{1} \frac{f(\xi)}{x^{-1}\xi} \sqrt{\frac{1+\xi}{1-\xi}} d\xi$$

APPENDIX VII

THE POSSIO KERNEL AND ITS APPROXIMATE REFRESENTATION AS A ROLYHOMIAL

1. Kussner (Ref. 4) gives for the kernel of the Possio integral equation the following expression:

(A7.01)
$$K(\lambda, z) = \frac{i\lambda e^{-iz}}{4\sqrt{1-\lambda^2}} \int_{-\infty}^{2/-\lambda^2} e^{iu} H_i [\lambda/u] \frac{du}{u}$$

where $H_{i}^{(2)}(x) = J_{i}(x) - iN_{i}(x)$, and J_{i} and N_{i} are the Bessel and Neumann functions of order unity in conventional notation.

The integral is only properly convergent when 2 <0, in which case

$$(A7.02) \quad H(\lambda,-2) = \frac{-i\lambda e^{i2}}{4\sqrt{1-\lambda^2}} \int_{2/\sqrt{2}}^{\infty} e^{-i\mu} H_i^{(a)}[\lambda u] \frac{du}{u}$$

In the case where z>ait is necessary to form the Cauchy principal value under the integral sign in equation (1.01), whence it is found that

(A7.03)
$$K(\lambda,z) = \frac{i\lambda e^{-iz}}{4\sqrt{1-\lambda^2}} \int_{z_{j-\lambda^2}}^{\infty} e^{iu} \mathcal{H}_{,[\lambda u]} \frac{du}{u}$$

By making use of the following identities which are easily proved by differentiation:

$$\left\{ e^{iu} H_{i}^{(a)}(\lambda u) \frac{du}{u} = \frac{\lambda^{2} I}{\lambda} e^{iu} H_{o}^{(a)}(\lambda u) du - \frac{i}{\lambda} e^{iu} H_{o}^{(a)}(\lambda u) - i\lambda H_{i}^{(a)}(\lambda u) \right\}$$

$$\left\{ e^{iu} H_{i}^{(a)}(\lambda u) \frac{du}{u} = \frac{\lambda^{2} I}{\lambda} e^{-iu} H_{o}^{(a)}(\lambda u) du + \frac{i}{\lambda} e^{-iu} H_{o}^{(a)}(\lambda u) + i\lambda H_{i}^{(a)}(\lambda u) \right\}$$

the following expanded forms of the Possio kernel are obtained:

$$\left\{ K(\lambda, z) = \frac{1}{4\sqrt{1-\lambda^{2}}} \left\{ e^{i\lambda w} \left[-H_{o}^{(a)}(w) + i\lambda H_{i}^{(a)}(w) \right] - i(1-\lambda^{2}) e^{-iz} \right\} e^{iu} H_{o}^{(a)}(\lambda u) du$$

$$\left\{ K(\lambda, z) = \frac{1}{4\sqrt{1-\lambda^{2}}} \left\{ e^{i\lambda w} \left[-H_{o}^{(a)}(w) - i\lambda H_{i}^{(a)}(w) \right] + i(1-\lambda^{2}) e^{-iu} H_{o}^{(a)}(\lambda u) du \right\} \right\}$$

where Z > 0, and $w = \frac{\lambda Z}{1-\lambda^2}$. Since

(A7.06)
$$\int_{0}^{\infty} e^{\pm iu} H_{o}(\lambda u) du = \frac{z}{\pi \sqrt{1-\lambda^{2}}} Log \frac{1+\sqrt{1-\lambda^{2}}}{\lambda},$$

the last integral in each expression may be written as

(A7.07)
$$\frac{2}{4\sqrt{1-\lambda^2}} \log \frac{1+\sqrt{1-\lambda^2}}{\lambda} - \int_{0}^{\sqrt{1-\lambda^2}} e^{\pm iu} H_0^{(2)}(\lambda u) du,$$

the latter form being more suitable for numerical computation. For $\lambda = 0$ it may be shown that

$$(A7.08) \begin{cases} 2\pi K(0,2) = -\frac{1}{Z} + ie^{-iZ} \left[C + \log Z + i \frac{\pi}{2} - \int_{0}^{Z} \frac{1 - e^{-iu}}{u} du \right] \\ 2\pi K(0,-2) = \frac{1}{Z} + ie^{iZ} \left[C + \log Z + i \frac{\pi}{2} - \int_{-L}^{Z} \frac{1 - e^{-iu}}{u} du \right] \end{cases}$$

where C = .577216 , known as Euler's constant, is defined as

(A7.09)
$$\lim_{n\to\infty} \left[1 + \frac{1}{2} + \frac{1}{3} + \dots + \frac{1}{n} - \log n \right]$$

2. The singularities of $K(\lambda, z)$

It is well known that as $x \to 0$ No(x) becomes infinite as $\log |x|$ and N₁(x) as 1/x. Thus in the vicinity of x = 0,

WADC TR 52-56

(A7.10)
$$H_{0}^{(2)}(x) = -\frac{2i}{\pi} L_{0}g(x) + \text{non-singular terms};$$

$$H_{1}^{(2)}(x) = \frac{2i}{\pi} \left[\frac{1}{2} \right] + \text{non-singular terms}.$$

Further, it is clear from the expanded form that these are the only singular terms. Affixing the proper coefficients to these terms as determined by equation (A7.05) gives

(A7.11)
$$K(\lambda, z) = \frac{1}{2\pi\sqrt{1-\lambda^2}} L_{xy}|z| - \frac{\sqrt{1-\lambda^2}}{2\pi} [1/z] + K_{x}(\lambda, z)$$

where $K_1(\lambda z)$ has no singularities. In Ref. 16 Schwartz has tabulated the values of $K_1(\lambda, z)$ for $\lambda z = 0$ in intervals of .1 and for $z = -2(1-\lambda^2)$ to $z = 2(1-\lambda^2)$ in intervals of (.02). Later in Ref. 17 the range of |z| for λz was extended to 5.1; for λz 8 and .9 to 2.00.

The singularities of K(0, Z) are, from (47.11) given by

(A7.12)
$$K(0,z) = \frac{i}{2\pi} Log |z| - \frac{1}{2\pi} [1/2] + K_1(0,z)$$

It follows that the difference

$$(A7.13) \ \overline{K}(\lambda,z) = K(\lambda,z) - \frac{1}{\sqrt{1-\lambda^2}} K(0,z) - \frac{\lambda^2}{2\pi/1-\lambda^2} [1/2] = K_1(\lambda,z) - \frac{1}{\sqrt{1-\lambda^2}} K_1(0,z)$$

is also non-singular. The real and imaginary parts of K are plotted in figure (A7.01) as functions of K for K =.7.

2. Representation of $\overline{K}(\lambda,z)$ as a polynomial.

Since K has singular derivatives at Z=0, it is not possible to represent it by a Taylor series expansion about this point. Further, even if such an expansion were possible, the retention of a finite number of terms would give a good approximation only for small values of Z, and more terms would be needed, the larger the Z range became. The range over which the value of Z extends is evidently -2 ω to 2ω , since $Z=\omega(-z)$ and Z and Z each have the range -1 to 1. It, therefore, appears that a more systematic scheme would be to obtain for K a representation such that over any arbitrarily chosen interval, the difference between the actual value and the approximate value were made as small as possible. One means of accomplishing this

is to represent \mathcal{R} over (say) the interval [-a to a] by Legendre polynomials:

The first few Legendre polynomials are:

(A7.15)
$$P_{1}(x) = x$$
 $P_{3}(x) = \frac{1}{2}(5x^{2} - 3x)$

The general expression for $R_{\bullet}(x)$ may be found in numerous sources (for example, Refs. 14 and 15). In Ref. 15 it is shown that the coefficients A_{77} may be determined from

(A7.16)
$$A_{n} = \frac{2n+1}{2a} \int_{-a}^{a} \bar{K}(z) P_{n}(z_{a}^{2}) dz$$

It can also be shown that with this representation, the mean square error, viz.

(A7.17)
$$E(z) = \int_{R=0}^{\infty} P_{R}(x_{0})^{2} dz$$

* is made a minimum. It is further noted that since a=24; equation (A7.16) defines the A_n as continuous functions of the reduced frequency, ω .

3. Evaluation of An

Since \mathcal{T}_n (%) is a polynomial of degree n in n, the evaluation of the n is reduced to the evaluation of integrals of the form

(A7.18)
$$\int_{-a}^{a} K(0,z)z^{p}dz$$

$$\int_{-a}^{a} K(\lambda,z)z^{p}dz \qquad , p=0,1,2,\cdots n$$

For h = 0 the value of the integral is defined as the Cauchy principal value, i. e.

(A7.19)
$$\int_{-a}^{a} K(\lambda, z) dz = \int_{-a}^{a} \{K(\lambda, z) - \frac{\sqrt{1-\lambda^2}}{2\pi} [\frac{1}{2}]\} dz$$
since
$$\int_{-a}^{a} \frac{dz}{z} = 0$$

The evaluation of the required integrals is easy for the case when $\lambda = 0$, since by differentiation of equation (A7.08),

(A7.20)
$$i\frac{d}{dz}[K_1(0,z)] = K(0,z) + \frac{1}{2\pi}[Y_2]$$
and so
$$= K_1(0,z) + \frac{6}{2\pi} Leg |z|$$

$$\int_{a}^{a} K(0,z) z^{n} dz = \int_{a}^{a} \left\{ K(0,z) + \frac{1}{2\pi} \left[\frac{1}{2} \right] \right\} dz - \frac{1}{2\pi} \int_{a}^{a} \frac{1}{2\pi} \left[\frac{1}{2} \right] dz$$
(A7.21)

$$=i\int_{-a}^{a}\frac{d}{dz}\left[K_{j}(z,z)\right]z^{n}dz-\frac{i}{z\pi}\int_{a}^{a}\left[\left(z\right)^{n}+\left(-z\right)^{n}\right]Logz\,dz$$

$$\int_{K_{1}(0,z)}^{A} Z^{n} dz = i \left[a^{n} K(g \circ) - (-a)^{n} K(o_{1} \circ) \right] - i n \int_{a}^{A} K(o_{1}z) z^{n-1} dz$$

$$- \frac{i}{2\pi} \frac{a^{n+1} - (-a)^{n+1}}{n+1} \left[Loga - \frac{1}{2\pi^{n+1}} \right]$$

For $\lambda \neq 0$, the expressions become more cumbersome. It is found after some calculation that

$$\int_{A}^{A} K_{i}(\lambda,z)dz = i \left[K(\lambda,a) - K(\lambda,-a)\right]$$

$$+ \frac{\lambda}{2\sqrt{1-\lambda^{2}}} \left\{\cos \frac{\lambda a}{1-\lambda^{2}} H_{i}^{(a)}\left(\frac{\lambda a}{1-\lambda^{2}}\right) - \lambda \sin \frac{\lambda a}{1-\lambda^{2}} H_{o}^{(a)}\left(\frac{\lambda a}{1-\lambda^{2}}\right) - (1-\lambda^{2})\right\}$$

$$- (1-\lambda^{2}) \int_{a}^{\frac{\lambda a}{1-\lambda^{2}}} H_{o}^{(a)}(u) \cos \lambda u \, du$$

For n 0 the integrals may be found by a recurrence relationship similar to (A7.22). The last integral constitutes the only unknown functions, but it can be shown by a process similar to that used in Appendix V, Section f that

$$(1-\lambda^{2}) \begin{cases} \frac{\lambda a}{-\lambda^{2}} & \text{(a) ide } \\ H_{0}(a)c & \text{de } = \frac{\lambda a}{\sqrt{1-\lambda^{2}}} \begin{cases} H_{0}(\lambda a) / (\frac{\lambda a}{1-\lambda^{2}}, cos^{-1}\lambda) \\ -iH_{1}(x) / (\frac{\lambda a}{1-\lambda^{2}}) / (\frac{-\lambda a}{1-\lambda^{2}}, cos^{-1}\lambda) \end{cases} + \frac{2}{4}\sqrt{1-\lambda^{2}} cos^{-1}\lambda$$

In view of the complexity of the expressions involved in the integration of $\mathcal{M}(\lambda, Z)$, the following alternative method was employed to obtain the results in the example of Part II of the report: In Reference 3, Dietze gives the following approximate expression for

where $\delta(\lambda, z)$ is a small regular remainder, the absolute value of which is never greater than (.2) in the range $-2 \le z \le 2$. For $-1 \le z \le 1$, the absolute value of δ is less than (.007). $R_{H} = R_{13} = 1$ and $R_{14} = 1$ are explicit functions of λ which are listed by Dietze on Page 26 of the reference above and are reproduced in Table (7.01). The numerical values of $R_{22} = R_{23} = 1$ are also given here for $\lambda = 0.3$, .4, .5, .6, ..7.

Since 5 is small, the error introduced by employing an approximate quadrature formula such as Simpson's rule will be negligible, while the remainder of the terms involve only simple functions which can at once be integrated. Using this method the value of

$$\int_{a}^{a} \overline{K}(\lambda,z) Z^{p} dz, (p - 0,1)$$

was calculated for λ = .7, and a = .1, .2, .3, .4, .5, .6, .7, .8, .9, 1.0. From these results the values of $\omega \omega_0$ and $\omega^2 \omega_0$ as listed in Table (2.01) were obtained.

TABLE (A7.01) (Reproduced from Reference 3)

$$\Delta K(\lambda, z) = K(\lambda, z) - K(0, z)$$

$$= \Delta K(\lambda, z) + \Delta K_2(\lambda, z)$$

$$\Delta K_{L}(\lambda, z) = \frac{R_{0}/z}{2} + \frac{A_{11}}{2} + \frac{R_{12}L_{0}g(z)}{2} + \frac{Z}{2}(R_{13} + R_{14}L_{0}g(z))$$

$$\Delta K_{L}(\lambda, z) = \frac{Z}{2} \frac{R_{2n}}{2} z^{n}$$

$$R_{10} = \frac{1}{4} \left(\frac{1-\sqrt{1-\lambda^{2}}}{1-\lambda^{2}} \right)$$

$$R_{11} = -\frac{1}{4} \left(\frac{1}{\sqrt{1-\lambda^{2}}} - 1 \right) - \frac{1}{2} \left[\frac{1}{\sqrt{1-\lambda^{2}}} \left[\frac{\lambda^{2} - \log(70/2(1-\lambda^{2}))}{1-\lambda^{2}} \right] + \log(70/4\sqrt{1-\lambda^{2}}) \right]$$

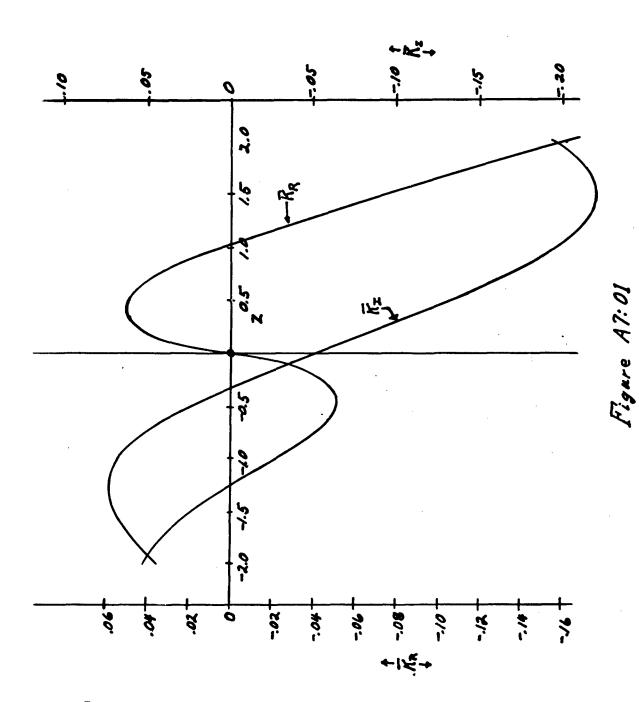
$$R_{12} = \frac{1}{2\pi} \left(\frac{1}{\sqrt{1-\lambda^{2}}} - 1 \right)$$

$$R_{13} = -\frac{1}{2\pi} \left\{ -1 + \log(70/4\sqrt{1-\lambda^{2}}) + \left[\frac{1}{\sqrt{1-\lambda^{2}}} \right] \left[1 - \frac{3}{2} \right] - \frac{1}{\sqrt{2}} - \frac{1}{\sqrt{2}} - \left(1 - \frac{3}{2} \right) \frac{1}{\sqrt{2}} \right] \right\}$$

$$- \frac{1}{4} \left(\frac{1}{2} + \frac{(3\lambda^{2} - 2)}{2(1-\lambda^{2})^{2}} \right)$$

$$R_{14} = -\frac{1}{24} \left[1 + (3N^2-2) \frac{1}{2(1-\lambda^2)^{3/2}} \right]$$
; Log $r = .5772.2 = \text{Bilar's Constant}$

λ	0,3	0,41	0,5	0,6	0,7
+10 ² k 22	0,0195	0,0872	0,3274	1,1811	4,7319
+10 ² k¹23	-0,0032	-0,0237	-0,1197	-0,4493	-2,8593
+10 ² k'24	0,0067	G,0021	-0,0047	-0,1054	-1,2914
+10 ² k'25	-0,0075	0,0122	0,0894	0,3478	3,2183
+10 ² k'26	-0.9013	0,0004	0,0033	0,0161	0,2452
+10 ² k'27	6,0039	-0,0055	-0,0409	-0,1468	-1,5321
+10 ² k'28	-0-0003	-0,0007	-0,0016	-0,0043	-0,0274
+10 ² k '2 9	-0,0004	0,0011	0,0070	0,0238	0,2539
+10 ² k'22	0,0419	0,1698	0,5484	1,6217	4,9165
+10 ² k''23	-0,0026	0,0137	0,0745	0,4830	2,2234
+102k 124	-0,020€	-0,1266	-0,4694	-1,5934	-6,5805
+10 ² k''25	0,0059	-0,0189	-0,0536	-0,3839	0,2119
+10 ² k" 26	0,0078	0,0553	0,2091	0,7325	3,0056
+10 ² k" 27	-0,0034	0,0119	0,0254	0,2153	-0,3464
+10 ² k" 28	-0,0011	-0,0086	-C,0326	-0,1184	-0,4719
+10 ² k* 29	0,0006	-0,0021	-0,0038	-0,0363	0,0677



The Non-Singular Mucleus Difference: $\vec{K}(\lambda,z) = K(\lambda,z) - \frac{1}{\sqrt{\lambda-\lambda^2}}K(0,z) - \frac{2\lambda^4}{2\pi\sqrt{(-\lambda^2)}}[1/z]$

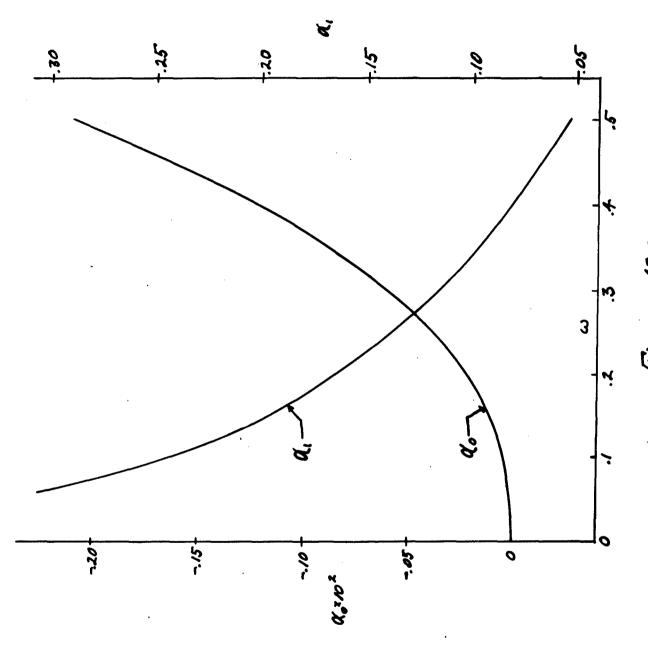
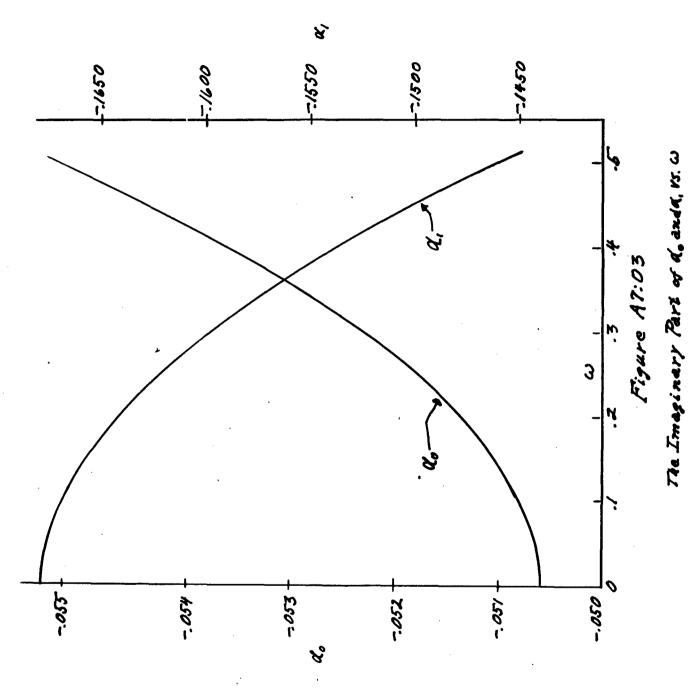


Figure A7:02
The Real Part of K. and K. vs. w



WADC TR 52-56

APPENDIX VIII

AUXILIARY TABLES

TABLE (A8.01)
THE FUNCTION $\mathcal{T}(\omega)$ (REF. 1)

ω ΄	7(ω)		
.05 .10 .20 .30 .40	.8180182612891 .6638483446041 .4551603772481 .3299423586381 .2499523299681 .1958723014191		

TABLE (A8.02) $e^{2\mu}e$ $e = .5 , \lambda = .7$

ω	JI.	6 ine	
.05 .10 .20 .30 .40	.0480392 .0960784 .1921569 .2882353 .3843137 .4803922	.9997115+.02401731 .9988460+.0480211 .9953880+.0959311 .9896330+.1436191 .9815950+.1909771 .9712910+.2378931	

TABLE (A8.03) $J_{p}(\mu)$ $\lambda = .7$

ω	<i>p</i> =0	10=1	10=2	
.05	.9994231	.0240127	.000288	
.10	.9976935	.0479838	.001153	
.20	.9907902	.0956357	.004602	
.30	.9793377	.1426262	.010313	
.40	.9634151	.1886311	.018241	
.50	.9431326	.2333334	.028282	
			2 ° 4	

DISTRIBUTION LIST

BAGR-OD, Attn: Mrs. D. Martin (4) DSC-SA (2) WCRRM-1 (25)

Bell Aircraft Corporation Niagara Falls, New York Attn: Leona Frame

Boeing Airplane Company Seattle 14, Washington Attn: Librarian

Beech Aircraft Corporation 6600 East Central Avenue Wichita 1, Kansas Attn: Frank H. Rogan

Bureau of Aeronautics Navy Department Washington 25, D. C.

California Institute of Technology Guggenheim Aeronautical Laboratory 1201 East California Street Pasadena 4, California Attn: Librarian

Cessna Aircraft Company Wichita, Kansas Attn: Thomas B. Salter

Chance Vought Aircraft Corporation
Dallas, Texas
Attn: Librarian
Thru: Bureau of Aeronautics
Navy Department
Washington 25, D. C.

Chase Aircraft Company, Incorporated Parkway & DeCou Avenues West Trenton, New Jersey University of Cincinnati Cincinnati 21, Ohio Attn: Professor Doty

Ì

Consolidated Vultee Aircraft Corporation San Diego Division San Diego, California Attn: Miriam S. Nylin, Librarian

Consolidated Vultee Aircraft Corporation Fort Worth Division Fort Worth 1, Texas Attn: E. Stanton Brown, Adm. Engr.

Cornell Aeronautical Laboratory 1455 Genesee Street Buffalo 5, New York Attn: Librarian, Elma Evans (1)

Douglas Aircraft Company, Incorporated 3000 Ocean Park Boulevard Santa Monica, California Attn: Librarian

Drexel Institute of Technology Philadelphia, Pennsylvania Attn: George Sonnemann

Fairchild Engine & Airplane Corporation Hagerstewn, Maryland Attn: Librarian

Grumman Aircraft Engineering Corporation Bethpage, Long Island, New York

Hughes Aircraft Company Division of Hughes Tool Company Florence Avenue & Teale Street Culver City, California Attn: Librarian

Leckhood Aircraft Corporation Factory A Post Office Box 551 Burbank, California Attn: Librarian Glenn L. Martin Company Baltimore 3, Maryland Attn: Librarian

Massachusetts Institute of Technology (2) 77 Massachusetts Avenue Cambridge 39, Massachusetts Attn: Professor Holt Ashley

McDonnell Aircraft Corporation St. Louis 21, Missouri Attn: Librarian

Midwest Research Institute h0h9 Pennsylvania Avenue Kanses City 2, Missouri Atta: Librarian

Morthrop Aircraft, Incorporated Morthrop Field Hawtherne, California Attn: Librarian

North American Aviation, Incorporated Los Angeles International Airport Los Angeles 45, California

National Advisory Committee for Aeronautics Langley Rir Ferce Base Hampton, Virginia Attn: Librarian

National Advisory Committee for Aeronautics Ames Aeronautical Laboratory Moffett Field, California

Polytechnic Institute of Brooklyn 99 Livingston Street Brooklyn 2, New York

Purdue University West Lafayette, Indiana Attn: Prefessor Hsu Lo

Princeton University Princeton, New Jersey

Republic Aviation Corporation Farmingdale, Long Island, New York Attn: Librarian Ryan Aeronautical Company Lindberg Drive San Diego 12, California Attn: Librarian

Southwest Research Institute P. O. Box 2296 San Antonio, Texas

Stanford University
Pale Alto, California

Sikorsky Aircraft Company Bridgeport 1, Connecticut

U. S. Department of Commerce Civil Aeronautics Administration Washington 25, D. C.

University of Colorado Boulder, Colorado Attn: Professor Sibert

University of California at Los Angeles Los Angeles 2h, California Attn: Librarian (1) John W. Miles (1) WADC TECH. REPT. 52-56 c.1

7